Intersection Control Evaluation

11th Ave SE at E Center St

City of Rochester, Olmsted County, Minnesota

City of Rochester



December 2018

SRF No. 018 11822

Intersection Control Evaluation

11th Ave SE at E Center St

City Engineer

Proposed Letting Date: TBD

Report Certification:

I hereby certify that this report was prepared by me or under my direct supervision and that I am a duly Licensed Professional Engineer under the laws of the State of Minnesota.

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|-------------------|----------|
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| Adrian S. Potter | 12/21/18 |
| Signature | Date |
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| City of Rochester | Date |

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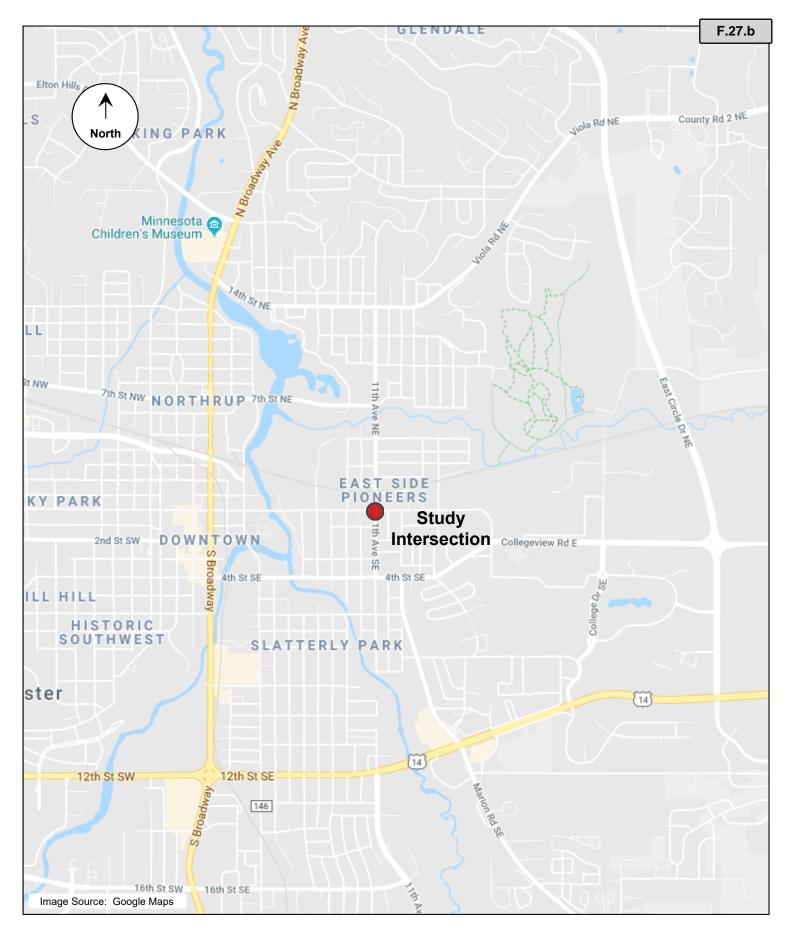
Introduction

This report comprises the intersection control evaluation results for the 11th Avenue SE at E Center Street intersection in the City of Rochester, Olmsted County, Minnesota (see Figure 1). The purpose of this evaluation was to analyze various intersection control alternatives under existing and future conditions to identify a preferred intersection control alternative. The intersection currently has a traffic signal that was installed in 1965. Since this signal is approximately 53 years old, it is likely nearing the end of its useful life. Therefore, the City determined there was a need to study this intersection in order to determine which form of intersection control would be best in the future. The following intersection control alternatives were considered applicable:

- Side-Street Stop Control
- All-Way Stop Control
- Traffic Signal Control
- Mini-Roundabout Control

Due to the age of the existing signal system, the traffic signal control alternative is defined as the replacement of the existing systems with a new system. Detailed warrants, operations, safety, and high-level cost analyses were performed to determine a preferred intersection control alternative. In addition to the above analyses, other factors considered applicable to determining the long-term preferred intersection control included:

- Right-of-Way Considerations
- Transportation System Considerations
- Pedestrian Considerations





Intersection Location

Figure 1

Intersection Control Evaluation 11th Avenue SE at E Center Street Rochester, Minnesota

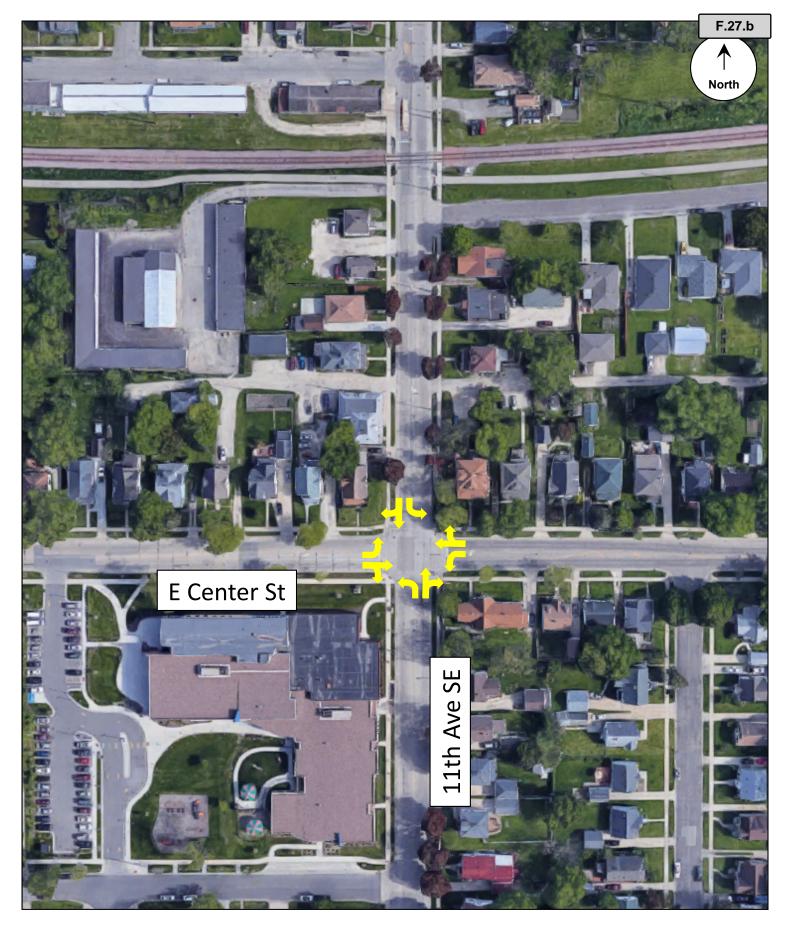
Intersection Characteristics

Existing Conditions

The 11th Avenue SE at E Center Street intersection is currently under traffic signal control. 11th Avenue SE and E Center Street are both two-lane undivided roadways with statutory speed limits of 30 mph (no posted speed limits). The adjacent area is comprised primarily of residential homes. The Boys and Girls Club of Rochester is located in the southwest quadrant of the intersection. The St. Francis of Assisi Church and School are located approximately four blocks south of the intersection. There is also an at-grade railroad crossing approximately 450 feet north of the intersection. Current intersection geometrics are listed below in Table 1 and shown in Figure 2.

Table 1. Existing Conditions

| Approach | Lane Configurations |
|------------------------|---|
| Northbound 11th Ave SE | One left-turn lane, one shared thru/right-turn lane |
| Southbound 11th Ave SE | One left-turn lane, one shared thru/right-turn lane |
| Eastbound E Center St | One left-turn lane, one shared thru/right-turn lane |
| Westbound E Center St | One left-turn lane, one shared thru/right-turn lane |





Existing Conditions

Figure 2

Intersection Control Evaluation 11th Avenue SE at E Center Street Rochester, Minnesota

Crash History

Crash data from 2006 through 2015 were obtained from the MnDOT Crash Mapping Analysis Tool (MnCMAT). When measuring crash data, the critical crash rate is a rate determined by MnDOT that is defined as statewide average rate adjusted for the specific volume of the subject intersection. If a crash rate exceeds the critical rate, it is highly recommended that action be taken to improve the safety at that intersection. 43 total crashes were reported at the study intersection during the ten-year analysis period. This results in a crash rate of 0.77 crashes per million entering vehicles, which is above the statewide average of 0.54 but below the critical value of 0.80 for similar intersections. The fatal and serious injury crash rate for the intersection was 1.80 crashes per 100 million entering vehicles. This is above the statewide average of 0.62 but below the critical rate of 2.87. A summary of the crash data is shown below and in Table 1:

- Crash Severity:
 - o 32 Property Damage Only Crashes
 - o 6 Possible Injury (Type C) Crashes
 - 4 Non-incapacitating Injury (Type B) Crashes
 - o 1 Fatal (Type K) Crash
- Crash Type:
 - o 5 Rear End Crashes

- o 4 Lost Control Crashes
- o 3 Overtaking Sideswipe Crashes
- o 27 Right-Angle Crashes

o 2 – Left-Turn Crashes

o 2 – Right-Turn Crashes

Table 2. Crash History Summary

| Location | Number | Daily Entering | Tota | l Crash Rate | e ⁽¹⁾ | Fatal & Ser | ious Injury Cra | sh Rate (2) |
|----------------------------------|---------------|-------------------|------------|--------------|------------------|-------------|-----------------|-------------|
| Location | of Crashes | Volume | Calculated | Average | Critical | Calculated | Average | Critical |
| 11th Ave SE at E Center St | 43 | 15,250 | 0.77 | 0.54 | 0.80 | 1.80 | 0.62 | 2.87 |

- (1) Intersection crash rates are expressed in crashes per million entering vehicles.
- (2) Intersection crash rates are expressed in crashes per 100 million entering vehicles.

Although the crash rate for the subject intersection is not above the critical rates, it is higher than the statewide average rates. This indicates there is a safety concern at this intersection. Based on these factors, it is desired that the proposed traffic control alternative at the intersection addresses the safety issues.

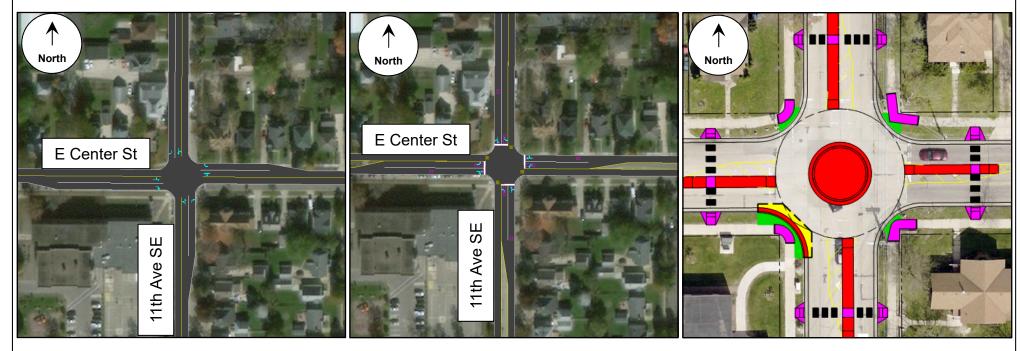
It should be noted that the crash data contains a high frequency of right-angle crashes and zero pedestrian crashes. These characteristics indicate that the existing pedestrian facilities are not a contributing factor the safety problem at the intersection. A high number of right-angle crashes is an uncommon characteristic for low-speed intersections and may help inform the recommendation of this report based on which alternative is expected to reduce that type of crash.

Future Conditions

Future lane configurations were developed to accommodate projected traffic volumes. For the sidestreet stop control and all-way stop control alternatives, all legs of the intersection were assumed to be given a dedicated right-turn lane. For the traffic signal control alternative, the existing lane configuration was assumed to remain. For the roundabout control alternative, a single-lane mini-roundabout was assumed. The assumed lane configurations for all alternatives are shown in Table 3. The assumed layouts for all alternatives are shown in Figure 3. A detailed concept drawing of the mini-roundabout alternative can be found in the Appendix.

Table 3. Future Intersection Lane Configurations

| Approach | Side-Street Stop and All-Way Stop Control Traffic Signal 6 | | Roundabout Control |
|------------------------|---|--|--|
| Northbound 11th Ave SE | One shared left- turn/thru laneOne right-turn lane | One left-turn laneOne shared thru/right-turn lane | One shared left- turn/thru/right-turn lane |
| Southbound 11th Ave SE | One shared left- turn/thru laneOne right-turn lane | One left-turn laneOne shared thru/right-turn lane | One shared left- turn/thru/right-turn lane |
| Eastbound E Center St | One shared left- turn/thru laneOne right-turn lane | One left-turn lane One shared thru/right-turn lane | One shared left- turn/thru/right-turn lane |
| Westbound E Center St | One shared left- turn/thru laneOne right-turn lane | One left-turn laneOne shared thru/right-turn lane | One shared left- turn/thru/right-turn lane |



Side-Street Stop and All-Way Stop Alternatives

Traffic Signal Alternative

Mini-Roundabout Alternative

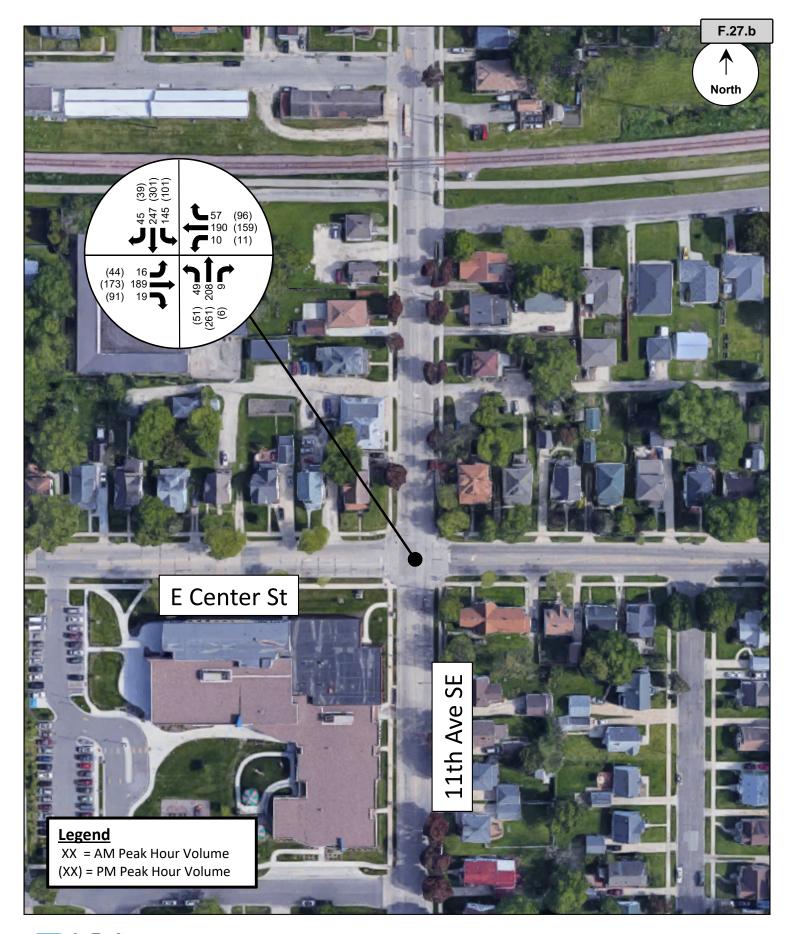


Figure 3

Traffic Volumes

Existing peak hour approach volumes at the study intersection were collected in October 2018 by SRF Consulting Group and are summarized in Figure 4. The existing turning movement counts are shown in the Appendix.

Forecast Year 2040 AM and PM peak hour turning movement volumes used in the analysis were based on existing hourly counts and further adjusted using historical AADT data to project future growth. Forecast Year 2040 turning movement volumes are shown in Figure 5.

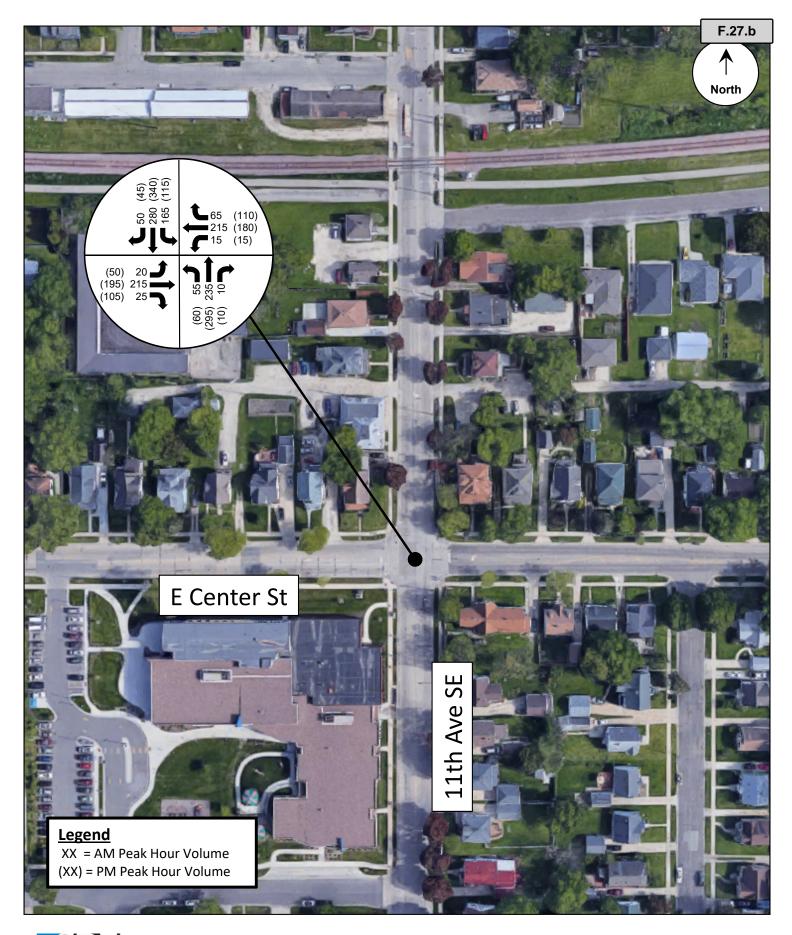




Existing Volumes

Figure 4

Intersection Control Evaluation 11th Avenue SE at E Center Street Rochester, Minnesota





Forecast Year 2040 Volumes

Figure 5

Intersection Control Evaluation 11th Avenue SE at E Center Street Rochester, Minnesota

Analysis of Alternatives

Warrants Analysis

A warrants analysis was performed for the traffic signal control alternative as outlined in the February 2018 *Minnesota Manual on Uniform Traffic Control Devices* (MnMUTCD). Analysis of signal warrants 1-3 was performed utilizing existing volumes. Signal warrants 6-8 were investigated and were determined to be not applicable to the study due to the lack of coordinated signal systems or roadway network concerns at the intersection.

Warrants 4, 5, and 9 were investigated further. Warrant 4 (Pedestrian Volume) was investigated due to the intersection's location within a residential area. Warrant 5 (School Crossing) was investigated due to the location of the Boys and Girls Club of Rochester in the southwest quadrant of the intersection as well as the St. Francis of Assisi School to the south. This facility was assumed to generate pedestrian behavior similar to that of a school. Warrant 9 (Intersection Near a Grade Crossing) was also investigated due to the railroad crossing approximately 450 feet north of the intersection.

Due to low pedestrian volumes recorded along with the turning movement counts, warrants 4 and 5 were not met by the intersection. Within the MnMUTCD, the figures relating to warrant 9 only contain data for grade crossings up to 130 feet from the subject intersection. Since the grade crossing is much farther away from the intersection than the MnMUTCD addresses, engineering judgement was used to determine that warrant 9 is also not met by the intersection. The lane geometry and approach speeds assumed for the warrant analysis are shown in Table 4.

Table 4. Warrants Analysis Assumptions

| Approach | Geometry | Speed Limit |
|------------------------|----------------------------|-------------|
| Northbound 11th Ave SE | Two or more approach lanes | 30 mph |
| Southbound 11th Ave SE | Two or more approach lanes | 30 mph |
| Eastbound E Center St | Two or more approach lanes | 30 mph |
| Westbound E Center St | Two or more approach lanes | 30 mph |

For the analysis, right turns on the minor approach were included as these turns are not given a dedicated lane and thus significantly impact the thru-movement on both minor approaches.

The 70 percent traffic volume factor was not used for the warrants analysis, as proposed conditions did not meet the necessary criteria (i.e. mainline roadway speed limits exceed 40 mph and the city population is less than 10,000). Table 5 provides a summary of the warrants analysis results, while the detailed volume-based warrants analysis is included in the Appendix.

In addition to the signal warrants, Multiway Stop Applications Warrant Condition C (MWSA C) was also evaluated as outlined in the MnMUTCD. The results of the MWSA warrants analysis are also shown in Table 5.

Table 5. Warrants Analysis Summary

| | Hours | Existing | Existing Volumes | | Volumes |
|--|----------------|--------------|------------------|--------------|-----------------|
| MnMUTCD Warrant | Required | Hours Met | Warrant Met? | Hours Met | Warrant Met? |
| MWSA C: Minimum Volumes | 8 | 13 | Yes | 14 | Yes |
| Warrant 1A: Minimum Vehicular Volume | 8 | 4 | No | 6 | No |
| Warrant 1B: Interruption of Continuous Traffic | 8 | 0 | No | 0 | No |
| Warrant 1C: Combination of Warrants | 8 | 1 | No | 4 | No |
| Warrant 2: Four-Hour Volume | 4 | 1 | No | 4 | Yes |
| Warrant 3B: Peak Hour Volume | 1 | 0 | No | 1 | Yes |
| Warrants 4, 5, 9 | Not Met | | | | |
| Warrants 6-8 | Not Applicable | | | | |

The results of the warrants analysis indicate the intersection meets MnMUTCD MWSA warrant C under existing conditions. However, the intersection does not meet any signal warrants under existing conditions. However, the results of the warrants analysis also indicate the intersection meets MnMUTCD MWSA warrant C and signal warrants 2 and 3B under 2040 conditions.

Based on guidance from Chapter 9 of MnDOT's Traffic Engineering Manual and references to Part 4 of MnDOT's Manual on Uniform Traffic Control Devices, signal removal analysis was conducted. Due to the intersection's failure to meet any signal warrants under existing conditions, a traffic signal removal analysis was conducted using 80% and 60% removal criteria. The volumes present within the intersection were first compared to 80% of the minimum warrant volumes. The results can be seen in Table 6.

Table 6. Signal Removal Analysis - 80% Removal Criteria

| MnMUTCD Warrant | Hours | 80% of Existing Requirements | | |
|--|----------|---------------------------------|-----------------|--|
| WINNOICD WARRANT | Required | Hours Met | Warrant Met? | |
| Warrant 1A: Minimum Vehicular Volume | 8 | 9 | Yes | |
| Warrant 1B: Interruption of Continuous Traffic | 8 | 1 | No | |
| Warrant 1C: Combination of Warrants | 8 | 6 | No | |

Note: Only signal warrant 1 is examined for signal removal analysis.

The results of the 80% removal criteria analysis indicate that the signal is warranted under 80% conditions. This result indicates that the signal likely should not be removed as it is functioning close to the signal warrant minimum volumes. Due to the signal satisfying the 80% warrant conditions, a 60% removal criteria analysis was not conducted.

Operations Analysis

Operational analysis of the side-street stop, all-way stop, and traffic signal control alternatives was performed using Synchro/SimTraffic. SimTraffic is a microscopic simulation software program that interfaces with Synchro and is used in this analysis. Traffic operations analysis of the roundabout alternative was conducted using RODEL and HCS software. RODEL is a software program that is based on existing roundabout operational research and uses an empirical formula method to determine roundabout delay based on geometric features and traffic flows. HCS is a software program that is based on equations and identities from the Highway Capacity Manual (HCM).

The operations analysis identifies a Level of Service (LOS) which indicates how well an intersection is operating based on delay per vehicle. Delay is calculated based on procedures outlined in the HCM. Intersections are given a ranking from LOS A to LOS F. LOS A indicates the best traffic operation and LOS F indicates an intersection where demand exceeds capacity. LOS A through LOS D are considered acceptable because the intersection would be operating under capacity. RODEL results for a Confidence Level (CL) of 50 percent and 85 percent were determined. 50 percent CL results are typically used for roundabout analysis while the 85 percent CL results indicate the sensitivity of the roundabout design. When a substantial degradation in LOS is expected from 50 percent CL to 85 percent CL, designers should exercise caution in the design of the roundabout to ensure adequate capacity is provided. A summary of the operational analysis under existing and 2040 conditions can be seen in Table 7 and Table 8, respectively. The detailed operational analysis results are shown in the Appendix.

Table 7. Operations Analysis Results - 2018 Conditions

| Alternative | | AM Pea | k Hour | PM Peak Hour | | |
|--------------------------|---------------|--------------------|--------|--------------------|-----|--|
| | Analysis Tool | Delay (sec/veh) | LOS | Delay (sec/veh) | LOS | |
| Side-Street Stop Control | SimTraffic | 9 / 20 | A/C | 12/31 | B/C | |
| All-Way Stop Control | SimTraffic | 13 / 17 | B/C | 16 / 23 | C/C | |
| Traffic Signal Control | SimTraffic | 9 / 10 | A/A | 10 / 11 | A/B | |
| | HCS 7 | 8/9 | A/A | 9 / 10 | A/A | |
| Roundabout Control | RODEL 50% CL | 7/8 | A/A | 7/8 | A/A | |
| | RODEL 85% CL | 11 / 15 | B/B | 13 / 16 | B/C | |

Note: Overall results are followed by the worst approach results.

Table 8. Operations Analysis Results - 2040 Conditions

| Alternative | | AM Peal | k Hour | PM Peak Hour | | |
|--------------------------|---------------|--------------------|--------|--------------------|-----|--|
| | Analysis Tool | Delay (sec/veh) | LOS | Delay (sec/veh) | LOS | |
| Side-Street Stop Control | SimTraffic | 22 / 52 | C/F | 34 / 99 | D/F | |
| All-Way Stop Control | SimTraffic | 22 / 37 | C/E | 38 / 77 | D/F | |
| Traffic Signal Control | SimTraffic | 10 / 11 | A/B | 11 / 11 | B/B | |
| | HCS 7 | 10 / 12 | A/B | 11 / 12 | B/B | |
| Roundabout Control | RODEL 50% CL | 8 / 11 | A/B | 9 / 10 | A/A | |
| | RODEL 85% CL | 17 / 26 | C/D | 19 / 24 | C/C | |

Note: Overall results are followed by the worst approach results.

Operational analysis results of existing conditions indicate that all alternatives are expected to perform with acceptable levels of service under proposed lane conditions. The side-street stop control alternative is expected to offer low average delays but higher minor-approach delays. The all-way stop control alternative is expected to operate with higher average delays but more evenly distributed delays than the side-street stop alternative. Both the traffic signal and roundabout control alternatives are expected to operate with low average and worst-approach delays. There is a significant difference between the RODEL 50% and 85% confidence level results. This indicates that the RODEL analysis is more susceptible to fluctuations in traffic volumes and could operate with less stability.

Operational analysis results of projected 2040 conditions indicate that both the side-street and all-way stop alternatives are expected to fail under future volumes. Both the traffic signal and roundabout control alternatives are still expected to operate with low average and worst-approach delays. There is still a significant difference between the RODEL 50% and 85% confidence level results under future conditions. This indicates that the RODEL analysis is more susceptible to fluctuations in traffic volumes and could operate with less stability.

It should be noted that operational analysis of the traffic signal alternative was conducted under the assumption that the existing signal phasing would remain. Due to low delay results for the traffic signal alternative under the existing phasing, models with alternative phasing were not considered. However, alternative signal phasing could potentially further improve operations under traffic signal control.

Safety Analysis

A safety analysis was performed to estimate the number of crashes per year for each traffic control alternative under current and 2040 conditions for the study intersection. For the traffic signal control alternative, the existing crash rate was assumed to remain. To analyze the crash rates for the side-street stop, all-way stop, and roundabout alternatives, the expected crash rates were assumed to be equal to the statewide average crash rates for similar intersections. A summary of the projected crashes per intersection alternative is shown in Table 9.

Table 9. Projected Crashes per Intersection Alternative

| Alternative | Intersection ADT | | | Projected Crashes/Year | | |
|-----------------------------|-----------------------|-----------------------|--------------------------------------|------------------------|-----------------------|--|
| | Existing Year 2018 | Forecast Year 2040 | Average Crash Rate ⁽¹⁾ | Existing Year 2018 | Forecast Year 2040 | |
| Side-Street Stop Control | | 17,000 | 0.19 (3) | 1.1 | 1.2 | |
| All-Way Stop Control | 15.050 | | 0.35 (4) | 1.9 | 2.2 | |
| Traffic Signal Control | 15,250 | | 0.77 (2) | 4.3 | 4.8 | |
| Roundabout Control | | | 0.32 (5) | 1.8 | 2.0 | |

- (1) Per million entering vehicles (2008-2017 data).
- (2) Assumed to match the current crash rate at the intersection.
- (3) Based on MnDOT Green Sheets average crash rate for urban thru/stop intersections.
- (4) Based on MnDOT Green Sheets average crash rate for all-way stop intersections.
- (5) Based on A Study of the Traffic Safety at Roundabouts in Minnesota (MnDOT Office of Traffic, Safety, and Technology).

Due to the presence of one fatal and four non-incapacitating injury crashes in the data, a fatal and serious injury crash analysis was also conducted.

Table 10. Projected Fatal & Serious Injury Crashes per Intersection Alternative

| Alternative | Intersection ADT | | | Projected Crashes/Year | | | |
|-----------------------------|-----------------------|-----------------------|--------------------------------------|------------------------|-----------------------|------|------|
| | Existing Year 2018 | Forecast Year 2040 | Average Crash Rate ⁽¹⁾ | Existing Year 2018 | Forecast Year 2040 | | |
| Side-Street Stop Control | | 17,000 | 0.35 ⁽³⁾ | 0.02 | 0.02 | | |
| All-Way Stop Control | 15.250 | | 17,000 | 15 250 17 000 | 0.60 (4) | 0.03 | 0.04 |
| Traffic Signal Control | 15,250 | | 1.80 ⁽²⁾ | 0.10 | 0.11 | | |
| Roundabout Control | | | 0.31 (5) | 0.02 | 0.02 | | |

- (1) Per 100 million entering vehicles (2008-2017 data).
- (2) Assumed to match the current fatal and serious injury crash rate at the intersection.
- (3) Based on MnDOT Green Sheets average fatal and serious injury crash rate for urban thru/stop intersections.
- (4) Based on MnDOT Green Sheets average fatal and serious injury crash rate for all-way stop intersections.
- (5) Based on A Study of the Traffic Safety at Roundabouts in Minnesota (MnDOT Office of Traffic, Safety, and Technology).

Based on the crash analysis, the side-street stop control alternative is expected to have the lowest crash rate while the roundabout control alternative is expected to have the lowest fatal and serious injury crash rate. The existing traffic signal control alternative is expected to have the least safety benefits for both rates. It should be noted that the majority of the crashes experienced at this intersection were right-angle/right-turn/left-turn crashes. These crashes are often caused by drivers not obeying or ignoring the existing signal system. Due to this behavioral trend at the intersection, it is reasonable to expect drivers to also ignore or fail to notice future stop signs. Thus, allowing drivers to decide their own right-of-way within a side-street or all-way stop design would likely lead to an increased number of right-angle crashes. It should also be noted that roundabouts typically have fewer conflict points than conventional intersections and that the geometry of a roundabout induces lower speeds for vehicles approaching and traversing an intersection. With lower speeds, the severity of the crashes is decreased. A roundabout should also eliminate almost all right-angle and left-turn type crashes as these movements are not possible within the geometry of a roundabout. Studies have shown the frequency of injury crashes is reduced more than property damage only crashes and that roundabout control significantly reduces the frequency of severe and fatal crashes.

Right-of-Way Considerations

No alternative would require additional right-of-way. Due to the lack of available right-of-way adjacent to the intersection, all alternatives must be able to fit within the existing right-of-way. The side-street stop, all-way stop, and traffic signal alternatives will not add any additional lanes in order to meet this requirement. The roundabout alternative was designed as a mini-roundabout capable of being constructed within the existing intersection footprint.

Transportation System Considerations

Currently, intersections in the area operate under either stop or signal control. However, there are roundabouts located within the City of Rochester and in Olmsted County, so traffic would likely be familiar with roundabout control.

The subject intersection is located between the bulk of downtown Rochester and a handful of large trip generating locations including the Olmsted Medical Center, Faud Mansour Sports Complex, and Rochester Community and Technical College campus. Due to this, the intersection is a contributing factor to the overall mobility to and from the eastern side of downtown Rochester.

Pedestrian Considerations

Based on the pedestrian volume data gathered with the turning movement counts, the subject intersection does not satisfy the pedestrian-based signal warrants. However, due to the intersection's location in urban Rochester, pedestrian volumes do exist and should be considered as part of the alternatives evaluation. Pedestrian movements would be difficult to accommodate under side-street stop conditions as pedestrians would be forced to wait for a gap in the 11th Avenue SE traffic in order to cross. Pedestrian movements would easily be accommodated under the all-way stop or traffic signal conditions as vehicles on all approaches are required to come to a stop fairly regularly. The traffic signal control alternative could offer increased pedestrian safety with dedicated pedestrian phasing. Pedestrian accommodations under roundabout control would operate similarly to the all-way stop control. There were no pedestrian-related crashes reported at the intersection within the last ten years. Thus, it can be assumed that pedestrian safety is not a significant issue under the current traffic signal control.

High-Level Cost Analysis

A high-level cost analysis was conducted for all alternatives. The results of this analysis can be seen in Table 11.

Table 11. High-Level Cost Analysis

| Alternative | Estimated Cost |
|--|----------------|
| Side-Street / All-Way Stop Control (1) | \$38,271 |
| Traffic Signal Control | \$284,000 |
| Roundabout Control | \$155,355 |

⁽¹⁾ Construction prices for the side-street and all-way stop control alternatives will vary by roughly \$2000 due to the difference in the number of stop and stop ahead signs between the alternatives.

This analysis indicates that the side-street/all-way stop alternatives would be significantly less expensive than the other two alternatives and that the traffic signal alternative would be significantly more expensive. It should be noted that the traffic signal alternative is not a "no-build" alternative but instead assumes a replacement of the existing system. A breakdown of the high-level cost analysis for all alternatives can be seen in the Appendix.

Conclusions

The following intersection control evaluation (ICE) conclusions and recommendations are provided for the 11th Avenue at E Center Street intersection in Rochester, Olmsted County, Minnesota:

• Warrants Analysis

The results of the warrant analysis under existing conditions indicate that while the intersection does satisfy the MWSA warrant. No signal warrants are met under existing volumes including the warrant for pedestrian volumes. However, the intersection does meet the 80% removal criteria for signals. This indicates that the signal could be retained since it is near the warrant minimums.

The results of the warrant analysis under 2040 conditions indicate that while the intersection does satisfy the MWSA warrant. Signal warrants 2 and 3B are met under 2040 volumes.

Operations Analysis

Operational analysis results indicate that all alternatives are expected to perform with acceptable levels of service under existing conditions. Both the traffic signal and mini-roundabout alternatives are expected to operate with low overall and worst-approach delays.

Operational analysis results indicate that both the side-street and all-way stop control alternatives are expected to fail under 2040 conditions. Both the traffic signal and mini-roundabout alternatives are expected to operate with low overall and worst-approach delays.

• Safety Analysis

Based on the crash analysis, the roundabout control alternative is expected to provide the lowest crash rate and fatal and serious injury crash rate. Both the side-street and all-way stop control alternatives are expected to significantly increase both the crash rate and the fatal and serious injury crash rate. Additionally, roundabouts all but eliminate right-angle crashes which comprise approximately 63% of the crashes reported at the subject intersection over the past ten years.

• High-Level Cost Analysis

The side-street/all-way stop control alternative is estimated to cost \$38,271. The traffic signal control alternative is expected to cost \$284,000. The roundabout control alternative is expected to cost \$155,355. This makes the side-street/all-way stop alternative the least expensive by a significant margin. However, both stop-controlled alternatives come with notable drawbacks in other areas.

Right-of-Way Considerations

All alternatives are not expected to require additional right-of-way.

Transportation System Considerations

Currently, there are a number of roundabouts located in Rochester. Traffic is expected to be familiar with the traversal of roundabouts. The subject intersection is a contributing factor to the mobility of the area between eastern and downtown Rochester.

• Pedestrian Considerations

Pedestrian accommodations would be difficult to include under side-street stop control conditions. Pedestrians would be afforded greater safety within the all-way stop, traffic signal, or mini-roundabout alternatives.

Recommended Intersection Control

A decision matrix was developed to help evaluate the key factors and is provided in Table 12.

A mini-roundabout design is recommended for the subject intersection. This recommendation is primarily based on the safety benefits afforded by a roundabout design. Due to the high frequency of right-angle crashes, a roundabout design should significantly reduce crashes overall at the intersection. Additionally, the roundabout alternative is expected to operate with similar delay values to the existing traffic signal alternative.

However, if the City of Rochester would rather not invest the amount of capital necessary to construct a roundabout, the conversion of the intersection to all-way stop control is also expected increase intersection safety. However, the all-way stop alternative should not be considered as a long-term solution due to its anticipated operational failure by 2040.

 Table 12.
 Alternative Decision Matrix

| Factor | | Side-Street Stop Control | All-Way Stop Control | Traffic Signal Control | Roundabout Control | Recommended Alternative(s) Based on Factor |
|---------------------|---------|---|--|--|---|--|
| | | | AWSC warrant | Signal warrants | | Side-Street Stop Control |
| | 2018 | • N/A | met under existing conditions | not met under existing conditions | • N/A | All-Way Stop Control |
| Warrant Analysis | | | Conditions | Conditions | | Roundabout Control |
| | 2040 | • N/A | AWSC warrant met under 2040 conditions | Signal warrants met under existing conditions | • N/A | All Alternatives |
| Operational | 2018 | Acceptable LOS | Acceptable LOS | Acceptable LOS | Acceptable LOS | All Alternatives |
| Analysis | 2040 | Unacceptable | Unacceptable | A | A | Traffic Signal Control |
| | 2040 | LOS | LOS | Acceptable LOS | Acceptable LOS | Roundabout Control |
| | Pro/e): | NI/A | Lower vehicle | Lower vehicle | Lower vehicle speeds | All-Way Stop Control |
| Safety Analysis | Pro(s): | • N/A | speeds | speeds | Eliminates right- angle crashes | Roundabout Control |
| Salety Allalysis | Con(s): | Higher mainline vehicle speedsLowest pedestrian safety | Drivers decide right-of-way | High existing crash rate | Drivers decide right-of-way | |
| High-Level Cost | Pro(s): | Least expensive | Least expensive | • N/A | Less expensive than signal | Side-Street Stop Control |
| Analysis | Con(s): | • N/A | • N/A | Most expensive | Significantly expensive | All-Way Stop Control |
| Right-of-Way | Pro(s): | No additional right-of-way required | No additional right-of-way required | No additional right-of-way required | No additional right-of-way required | All Alternatives |
| Considerations | Con(s): | • N/A | • N/A | • N/A | • N/A | |
| | Dro/o\: | - N/A | Capable of providing | Capable of dedicated | Capable of providing | All-Way Stop Control |
| Pedestrian | Pro(s): | • N/A | pedestrian accommodations | pedestrian phasing | pedestrian accommodations | Roundabout Control |
| Considerations | Con(s): | Pedestrians must find gaps in E Center St traffic | • N/A | • N/A | • N/A | |

Appendix

- Year 2018 Intersection Turning Movement Data
- 2006-2015 Crash Data
- 2018 Warrant Analysis
- 2040 Warrant Analysis
- Signal Warrant Analysis 80% Removal Criteria
- Detailed 2018 Operations Analysis
- Detailed 2040 Operations Analysis
- Mini-Roundabout Alternative Layout
- High-Level Cost Estimates

Year 2018 Intersection Turning Movement Data

SRF Consulting Group Turning Movement Count

| Start | | 11th A E | | | | 11th A | ve NE | | | E Cer N | | | | E Cen Si | | | 15 min Veh. | 15 min Ped |
|--------------|-----|-------------|----------|-----|---|----------|----------|--------|---------|------------|----------|-----|----------|-------------|--------|-----|----------------|---------------|
| Time | L | Т | | Ped | L | т '' | R | Ped | L | т `` | R | Ped | L | T | R | Ped | Total | Total |
| 600 | - | 14 | 2 | - | 1 | 19 | 7 | - | 3 | 10 | - | - | 7 | 24 | 5 | - | 92 | - |
| 615 | - | 16 | 2 | - | 1 | 29 | 4 | | 6 | 25 | - | - | 3 | 28 | 4 | - | 118 | - |
| 630 | - | 18 | 2 | 2 | - | 52 | 11 | - | 14 | 16 | - | - | 14 | 35 | 6 | - | 168 | 2 |
| 645 | 5 | 28 | 4 | - | | 47 | 13 | | 18 | 30 | 1 | 1 | 20 | 37 | 12 | - | 215 | - |
| 700 | 3 | 34 | 8 | - | 5 | 45 | 14 | | 17 | 44 | - | - | 13 | 40 | 4 | - | 227 | - |
| 715 | 4 | 33 | 3 | - | 3 | 52 | 11 | - | 11 | 54 | 2 | - | 32 | 56 | 13 | 1 | 274 | 1 |
| 730 | 5 | 51 | 3 | - | 1 | 63 | 14 | - | 18 | 63 | 2 | - | 41 | 69 | 14 | 2 | 344 | 2 |
| 745 | 5 | 63 | 4 | 1 | 3 | 42 | 17 | - | 10 | 47 | | - | 41 | 76 | 11 | 1 | 319 | 2 |
| 800 | 2 | 42 | 9 | - | 3 | 33 | 15 | - | 10 | 44 | 5 | - | 31 | 46 | 7 | - | 247 | - |
| 815 | 3 | 31 | 7 | - | - | 26 | 16 | - | 14 | 31 | - | - | 21 | 65 | 10 | - | 224 | - |
| 830 845 | 4 2 | 30 | 11 | - | 3 | 23 30 | 14 10 | 1 | 21 | 45 49 | 2 | - | 13 | 67 | 5 | - | 236 | 1 |
| | | 23 | 4 | - 1 | 1 | | 15 | | 11 | 49 | | - | 20 | 59 48 | 4 | - | 215 | |
| 900 915 | 8 | 23 45 | 5 2 | 1 | 3 | 27 10 | 12 | - | 12 6 | 43 | 3 | - | 25 26 | 48 54 | 9 | - | 222 218 | 1 |
| 930 | 4 | 31 | 8 | - | 2 | 15 | 15 | 1 | 8 | 36 | 1 | - | 20 | 43 | 9 | - | 192 | 1 |
| 930 | 1 | 23 | 12 | - | 1 | 26 | 16 | 2 | 4 | 40 | <u> </u> | - | 13 | 37 | 3 | - | 176 | 2 |
| 1000 | 3 | 23 | 9 | | 3 | 20 | 10 | - | 6 | 32 | 1 | - | 11 | 36 | 4 | _ | 158 | |
| 1015 | 2 | 21 | 9 | _ | 1 | 18 | 13 | _ | 8 | 38 | 1 | - | 11 | 40 | 8 | _ | 170 | _ |
| 1030 | 6 | 27 | 8 | _ | 2 | 22 | 16 | - | 7 | 38 | <u> </u> | - | 16 | 43 | 8 | - | 193 | _ |
| 1045 | 5 | 37 | 6 | 1 | - | 17 | 20 | | 5 | 45 | 2 | - | 22 | 47 | 10 | _ | 216 | 1 |
| 1100 | 4 | 12 | 12 | 4 | 3 | 26 | 8 | - | 5 | 46 | 2 | - | 10 | 51 | 5 | - | 184 | 4 |
| 1115 | - | 15 | 10 | 1 | 3 | 26 | 12 | - | 10 | 47 | 2 | - | 10 | 49 | 3 | 1 | 187 | 2 |
| 1130 | 4 | 20 | 5 | _ | 1 | 23 | 18 | 1 | 8 | 37 | 4 | - | 18 | 45 | 3 | _ | 186 | 1 |
| 1145 | 4 | 28 | 12 | 1 | 1 | 30 | 27 | | 6 | 48 | 4 | - | 29 | 36 | 7 | - | 232 | 1 |
| 1200 | 8 | 27 | 6 | - | 2 | 39 | 34 | - | 4 | 49 | 1 | - | 22 | 51 | 7 | - | 250 | - |
| 1215 | 1 | 21 | 11 | - | 1 | 46 | 29 | 1 | 7 | 40 | - | - | 19 | 39 | 8 | 1 | 222 | 2 |
| 1230 | 3 | 25 | 9 | 1 | 1 | 16 | 23 | | 7 | 31 | 3 | - | 18 | 45 | 6 | - | 187 | 1 |
| 1245 | 6 | 26 | 8 | - | 1 | 27 | 18 | - | 10 | 50 | 3 | - | 29 | 51 | 8 | - | 237 | - |
| 1300 | 7 | 20 | 7 | 1 | 5 | 28 | 25 | - | 9 | 41 | - | - | 19 | 36 | 7 | - | 204 | 1 |
| 1315 | 2 | 18 | 13 | 2 | 2 | 25 | 16 | - | 8 | 53 | 2 | 2 | 17 | 38 | 4 | - | 198 | 4 |
| 1330 | 7 | 26 | 7 | - | 2 | 41 | 13 | - | 9 | 39 | 1 | - | 16 | 40 | 5 | - | 206 | - |
| 1345 | 3 | 24 | 8 | - | 2 | 49 | 22 | - | 11 | 41 | 2 | - | 16 | 46 | 7 | - | 231 | - |
| 1400 | 3 | 25 | 5 | - | 3 | 45 | 22 | - | 7 | 56 | 6 | - | 11 | 39 | 8 | - | 230 | - |
| 1415 1430 | 9 | 29 22 | 11 11 | 1 | 3 | 28 29 | 20 17 | - 1 | 6 5 | 53 51 | - | - | 24 16 | 58 65 | 7 6 | 1 | 246 234 | 3 |
| 1445 | 5 | 30 | 15 | 4 | 2 | 39 | 22 | - | 9 | 66 | 1 | 1 | 16 | 70 | 5 | ı | 280 | 5 |
| 1500 | 5 | 30 | 15 | 1 | 2 | 34 | 16 | 1 | 6 | 58 | 2 | - | 26 | 70 | 11 | 1 | 275 | 3 |
| 1515 | 9 | 38 | 31 | 1 | 5 | 29 | 22 | - | 10 | 56 | - | _ | 26 | 97 | 11 | 1 | 334 | 2 |
| 1530 | 15 | 53 | 27 | - 1 | 2 | 49 | 27 | - | 20 | 81 | 5 | 1 | 20 | 67 | 13 | 1 | 380 | 1 |
| 1530 | 10 | 47 | 14 | 1 | 1 | 49 | 19 | - | 12 | 66 | 1 | - 1 | 34 | 71 | 9 | - | 380 | 1 |
| 1600 | 10 | 35 | 19 | - 1 | 3 | 40 | 28 | 1 | 9 | 58 | <u> </u> | 1 | 20 | 66 | 6 | - | 295 | |
| 1615 | 10 | 51 | 16 | - | 2 | 29 | 20 | 1 | 10 | 72 | 2 | - | 27 | 76 | 4 | - | 319 | 1 |
| 1630 | 11 | | 23 | | 3 | 36 | 30 | 2 | 9 | 64 | 4 | 1 | 24 | 64 | 7 | 2 | 327 | 5 |
| | | 52 47 | | | | | | | | | | | | | | | | 1 |
| 1645 | 7 | 47 | 16 | 1 | 5 | 37 | 23 27 | - | 8 | 61 | - 2 | - 1 | 16 | 67 | 4 5 | - | 291 | 1 |
| 1700 | 8 | 48 | 17 | - | 2 | 43 | | | 12 | 72 | 3 4 | 1 | 31 | 69 | | - | 337 | |
| 1715 | 16 | 51 | 13 | - | 2 | 36 | 19 | 2 | 5 | 77 | | 2 | 21 | 73 | 5 | 2 | 322 | 6 |
| 1730 | 10 | 37 | 14 | - | 3 | 32 | 12 | 1 | 8 | 61 | - | - | 15 | 53 | 5 | - | 250 | 1 |
| 1745 | 7 | 31 | 14 | - | 3 | 14 | 11 | - | 3 | 66 | 4 | 1 | 15 | 67 | 10 | 1 | 245 | 2 |
| 1800 | 5 | 17 | 9 | - | 1 | 47 | 19 | - | 9 | 46 | 1 | - | 10 | 51 | 11 | - | 226 | |
| 1815 | 7 | 16 | 11 | 1 | 4 | 21 | 11 | - | 8 | 53 | 1 | - | 11 | 47 | 8 | - | 198 | 1 |
| 1830 | 6 | 17 | 9 | - | 2 | 11 | 13 | - | 3 | 71 | 1 | 1 | 6 | 62 | 2 | 2 | 203 | 3 |
| 1845 | 8 | 17 | 8 | - | 2 | 18 | 5 | - | 5 | 49 | 2 | - | 11 | 52 | 4 | - | 181 | - |

SRF Consulting Group Turning Movement Count

| | | 11th A | | | | 11th A | | | | E Cer | | | | E Cer | | | 15 min | 15 min |
|--------|------|--------|------|-----|------|--------|------|-----|------|-------|------|-----|------|-------|------|-----|--------|----------|
| Start | | E | | | | W | | | | N | | | | S | | | Veh. | Ped |
| Time | L | T | R | Ped | L | T | R | Ped | L | T | R | Ped | L | T | R | Ped | Total | Total |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| Peak 1 | 0000 | to | 1000 | | | | | | | | | | | | | | | |
| 715 | 4 | 33 | 3 | - | 3 | 52 | 11 | - | 11 | 54 | 2 | - | 32 | 56 | 13 | 1 | 274 | - |
| 730 | 5 | 51 | 3 | - | 1 | 63 | 14 | - | 18 | 63 | 2 | - | 41 | 69 | 14 | 2 | 344 | 1 |
| 745 | 5 | 63 | 4 | 1 | 3 | 42 | 17 | - | 10 | 47 | - | - | 41 | 76 | 11 | 1 | 319 | 2 |
| 800 | 2 | 42 | 9 | - | 3 | 33 | 15 | - | 10 | 44 | 5 | - | 31 | 46 | 7 | - | 247 | - |
| Total | 16 | 189 | 19 | 1 | 10 | 190 | 57 | - | 49 | 208 | 9 | - | 145 | 247 | 45 | 4 | 1,184 | 3 |
| PHF | 0.80 | 0.75 | 0.53 | | 0.83 | 0.75 | 0.84 | | 0.68 | 0.83 | 0.45 | | 0.88 | 0.81 | 0.80 | | 0.86 | |
| Trucks | - | 1% | - | - | 10% | 2% | - | - | - | 2% | 11% | - | 1% | 3% | - | - | 2% | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| Peak 2 | 1000 | to | 1400 | | | | | | | | | | | | | | | |
| 1400 | 3 | 25 | 5 | - | 3 | 45 | 22 | - | 7 | 56 | 6 | - | 11 | 39 | 8 | - | 230 | - |
| 1415 | 9 | 29 | 11 | - | 1 | 28 | 20 | - | 6 | 53 | - | - | 24 | 58 | 7 | - | 246 | - |
| 1430 | 9 | 22 | 11 | 1 | 3 | 29 | 17 | 1 | 5 | 51 | - | - | 16 | 65 | 6 | 1 | 234 | 1 |
| 1445 | 5 | 30 | 15 | 4 | 2 | 39 | 22 | - | 9 | 66 | 1 | 1 | 16 | 70 | 5 | - | 280 | 5 |
| Total | 26 | 106 | 42 | 5 | 9 | 141 | 81 | 1 | 27 | 226 | 7 | 1 | 67 | 232 | 26 | 1 | 990 | 6 |
| PHF | 0.72 | 0.88 | 0.70 | | 0.75 | 0.78 | 0.92 | | 0.75 | 0.86 | 0.29 | | 0.70 | 0.83 | 0.81 | | 0.88 | |
| Trucks | 8% | 5% | 2% | - | - | 2% | 2% | - | - | 4% | - | - | 1% | 4% | 4% | - | 3% | |
| | . " | | | | | | | | | | | | ' | | | | | <u>.</u> |
| | | | | | | | | | | | | | | | | | | |
| Peak 3 | 1400 | to | 2400 | | | | | | | | | | | | | | | |
| 1515 | 9 | 38 | 31 | 1 | 5 | 29 | 22 | - | 10 | 56 | - | - | 26 | 97 | 11 | 1 | 334 | 2 |
| 1530 | 15 | 53 | 27 | - | 2 | 49 | 27 | - | 20 | 81 | 5 | 1 | 21 | 67 | 13 | - | 380 | 1 |
| 1545 | 10 | 47 | 14 | 1 | 1 | 40 | 19 | - | 12 | 66 | 1 | - | 34 | 71 | 9 | - | 324 | 1 |
| 1600 | 10 | 35 | 19 | - | 3 | 41 | 28 | 1 | 9 | 58 | - | 1 | 20 | 66 | 6 | - | 295 | 2 |
| Total | 44 | 173 | 91 | 2 | 11 | 159 | 96 | 1 | 51 | 261 | 6 | 2 | 101 | 301 | 39 | 1 | 1,333 | 6 |
| PHF | 0.73 | 0.82 | 0.73 | | 0.55 | 0.81 | 0.86 | | 0.64 | 0.81 | 0.30 | | 0.74 | 0.78 | 0.75 | | 0.88 | |
| Trucks | 7% | 2% | 1% | - | 27% | 1% | - | - | - | 4% | - | _ | 3% | 3% | 3% | - | 3% | |

2006-2015 Crash Data

Intersection Safety Screening

Intersection: 11th Avenue SE at E Center Street

Crash Data, 2006-2015.



| Crashes by Crash Severity | | | | | | | | | |
|---------------------------|----|--|--|--|--|--|--|--|--|
| Fatal | 1 | | | | | | | | |
| Incapacitating Injury | 0 | | | | | | | | |
| Non-incapacitating Injury | 4 | | | | | | | | |
| Possible Injury | 6 | | | | | | | | |
| Property Damage | 32 | | | | | | | | |
| Total Crashes | 43 | | | | | | | | |

| Intersection Characteristics | | | | | | | | | | | | |
|------------------------------|---------|--|--|--|--|--|--|--|--|--|--|--|
| Entering Volume | 15,250 | | | | | | | | | | | |
| Traffic Control | Signals | | | | | | | | | | | |
| Environment | Urban | | | | | | | | | | | |
| Speed Limit | 30 mph | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |

Annual crash cost = \$256,120

Statewide Comparison

| Total Crash Rate | | | | | | | | | | |
|-------------------|------|--|--|--|--|--|--|--|--|--|
| Observed | 0.77 | | | | | | | | | |
| Statewide Average | 0.54 | | | | | | | | | |
| Critical Rate | 0.80 | | | | | | | | | |
| Critical Index | 0.96 | | | | | | | | | |

| Signals: | low vo | lume, i | low s | peed |
|----------|--------|---------|-------|------|
|----------|--------|---------|-------|------|

| Fatal & Serious Injury Crash Rate | | | | | | | | | |
|-----------------------------------|------|--|--|--|--|--|--|--|--|
| Observed | 1.80 | | | | | | | | |
| Statewide Average | 0.62 | | | | | | | | |
| Critical Rate | 2.87 | | | | | | | | |
| Critical Index | 0.63 | | | | | | | | |

The observed crash rate is the number of crashes per million entering vehicles (MEV). The critical rate is a statistical comparison based on similar intersections statewide. An observed crash rate greater than the critical rate indicates that the intersection operates outside the expected, normal range. The critical index reports the magnitude of this difference.

The observed total crash rate for this period is 0.77 per MEV; this is 4% below the critical rate. Based on similar statewide intersections, an additional 2 crashes over the ten years would indicate this intersection operaters outside the normal range.

The observed fatal and serious injury crash rate for this period is 1.80 per 100 MEV; this is 37% below the critical rate. The intersection operates within the normal range.

2018 Warrant Analysis



WARRANTS ANALYSIS

Intersection Control Evaluation

Existing Year 2018 11th Ave SE at E Center St

City of Rochester, Olmstead County

| פר | Location: City of Rochester, Olmstead Cou | inty Speed (mph) | Lanes | | Approach |
|-----------|---|------------------|-----------|-------------------|------------------------|
| 를 들 | Date: 10/17/2018 | 30 | 2 or more | Major Approach 1: | Northbound 11th Ave SE |
| kgrc | Analysis Prepared By: Kevin Olm | 30 | 2 or more | Major Approach 3: | Southbound 11th Ave SE |
| 9. ن | Population Less than 10,000: No | 30 | 2 or more | Minor Approach 2: | Eastbound E Center St |
| Ba Inf | Seventy Percent Factor Used: No | 30 | 2 or more | Minor Approach 4: | Westbound E Center St |

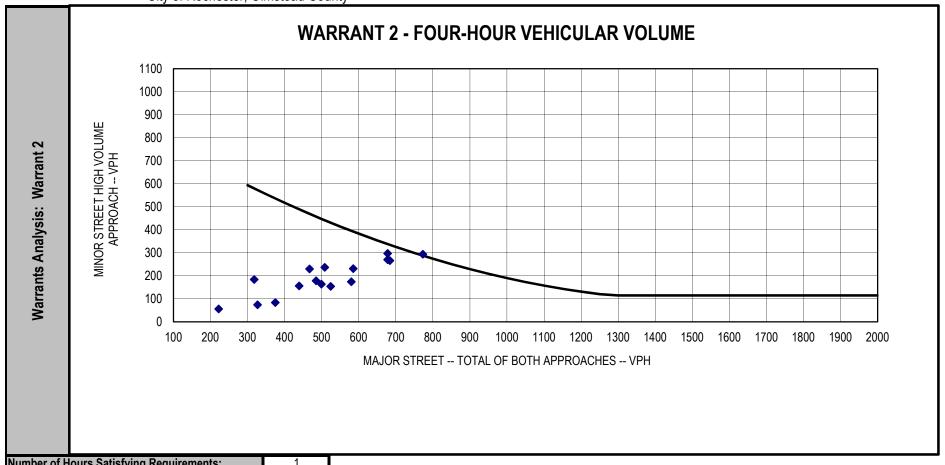
| | | Major | Major | Total | Warra | nt Met | Minor | Minor | Largest | Warra | nt Met | Met Sam | ne Hours | Comb | ination | MWS | A (C) |
|--------------------|---------------------------------------|--|--------------|-------|-------|--------|------------|------------|------------|---------|--------|-------------|---------------|----------|------------|-----|-------|
| (2) | Hour | Approach 1 | Approach 3 | 1+3 | 600 | 900 | Approach 2 | Approach 4 | Minor App. | 200 | 100 | Condition A | Condition B | Α | В | 300 | 200 |
| 10 | 6 - 7 AM | 123 | 195 | 318 | | | 91 | 184 | 184 | | Х | | | | | Χ | Х |
| and | 7 - 8 AM | 268 | 410 | 678 | X | | 216 | 270 | 270 | Χ | Х | Х | | X | | Χ | Χ |
| a B | 8 - 9 AM | 232 | 348 | 580 | | | 168 | 174 | 174 | | Х | | | Χ | | Х | Χ |
| , 18 | 9 - 10 AM | 205 | 294 | 499 | | | 164 | 145 | 164 | | Х | | | Χ | | Х | Χ |
| 4, | 10 - 11 AM | 183 | 256 | 439 | | | 156 | 142 | 156 | | Х | | | | | Х | X |
| ts t | 11 - 12 AM | 219 | 266 | 485 | | | 126 | 178 | 178 | | Х | | | Х | | Х | X |
| Warrants | 12 - 1 PM | 205 | 303 | 508 | | | 151 | 237 | 237 | X | Х | | | Х | | X | Χ |
| arı | 1 - 2 PM | 216 | 251 | 467 | | | 142 | 230 | 230 | X | Х | | | | | X | Χ |
| _ | 2 - 3 PM | 260 | 325 | 585 | | | 174 | 231 | 231 | X | Х | | | Х | | X | Χ |
| Warrants Analysis: | 3 - 4 PM | 317 | 456 | 773 | X | | 294 | 246 | 294 | X | Х | Х | | Х | Х | X | Χ |
| lys | 4 - 5 PM | 297 | 381 | 678 | X | | 297 | 257 | 297 | X | Х | Х | | Х | | X | Χ |
| nal | 5-6 PM | 315 | 369 | 684 | X | | 266 | 204 | 266 | X | Х | Х | | Х | | X | Х |
| | 6 - 7 PM | 249 | 275 | 524 | | | 130 | 154 | 154 | | X | | | | | X | Х |
| l ti | 7 - 8 PM | 172 | 203 | 375 | | | 84 | 69 | 84 | | | | | | | X | |
| ra | 8-9 PM | 173 | 154 | 327 | | | 74 | 60 | 74 | | | | | | | X | |
| Na | 9 - 10 PM | 113 | 109 | 222 | | | 56 | 44 | 56 | | | | | | | | |
| _ | 10 - 11 PM | 0 | 0 | 0 | | | 0 | 0 | 0 | | | | | | | | |
| | | | | | | | | | | | | 4 | 0 | 9 | 1 | 1 | 3 |
| | | | and Descript | | | | Hours | | Hours | Require | ed | | | t/Not Me | | | |
| > | MWSA (C): | Multiway Stop | | | on C | | 13 | 3 | | 8 | | | Met - Multiwa | | Applicatio | ns | |
| ant ar | | Minimum Veh | | | | | 4 | | | 8 | | | | Not Met | | | |
| Warrant Summary | | Varrant 1B: Interruption of Continuous Traffic | | | | | 0 8 | | | | | | Not Met | | | | |
| | | Combination | | | | | 1 | | | 8 | | | | Not Met | | | |
| | Warrant 2: Four-Hour Vehicular Volume | | | | | | 1 | | | 4 | | | | Not Met | | | |
| | Warrant 3B: | Peak Hour | | | | | 0 | | | 1 | | | | Not Met | | | |



WARRANTS ANALYSIS

Existing Year 2018

11th Ave SE at E Center St Intersection Control Evaluation City of Rochester, Olmstead County



Number of Hours Satisfying Requirements:

Notes:

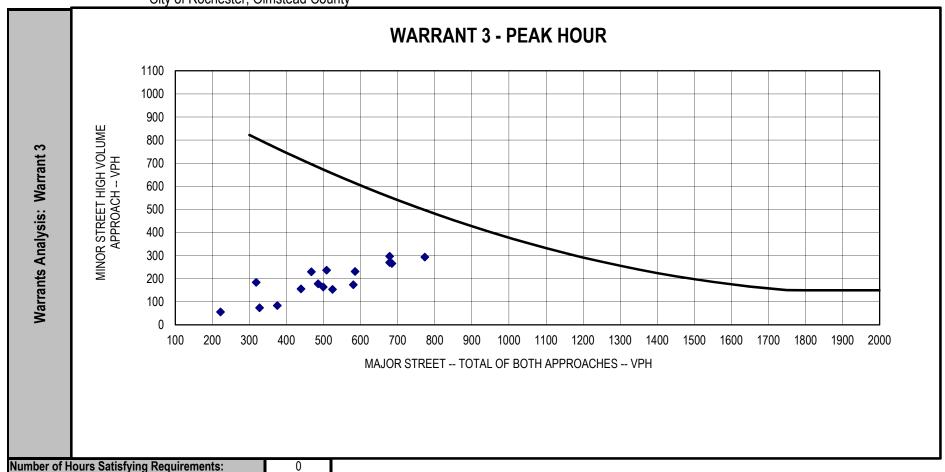
1. 115 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACH WITH TWO OR MORE LANES AND 80 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.



WARRANTS ANALYSIS

Existing Year 2018

11th Ave SE at E Center St Intersection Control Evaluation City of Rochester, Olmstead County



Notes:

1. 150 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACH WITH TWO OR MORE LANES AND 100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

2040 Warrant Analysis



Forecasted Year 2040

11th Ave SE at E Center St Intersection Control Evaluation City of Rochester, Olmstead County

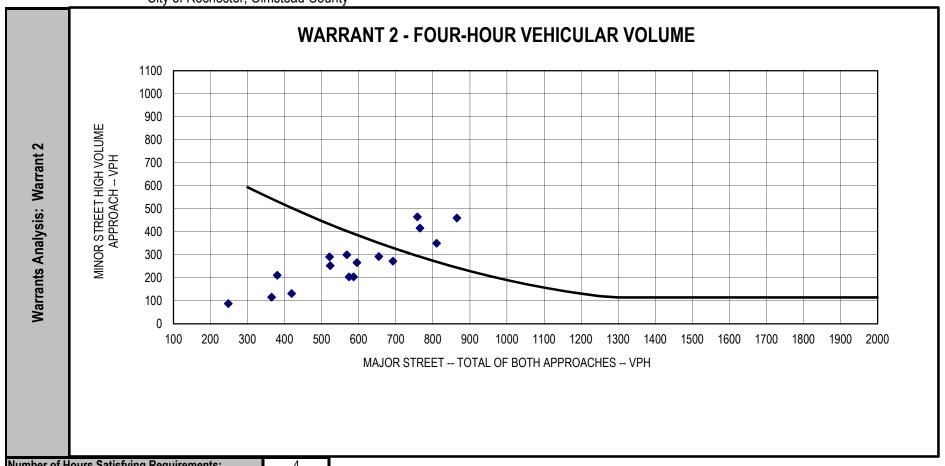
| pr u | Location: City of Rochester, Olmstead | County | Speed (mph) | Lanes | | Approach |
|---------|---------------------------------------|--------|-------------|-----------|-------------------|------------------------|
| l jë jë | Date: 10/25/2018 | | 30 | 2 or more | Major Approach 1: | Northbound 11th Ave SE |
| kgrc | Analysis Prepared By: Kevin Olm | | 30 | 2 or more | Major Approach 3: | Southbound 11th Ave SE |
| O. O | Population Less than 10,000: | No | 30 | 2 or more | Minor Approach 2: | Eastbound E Center St |
| Ba | Seventy Percent Factor Used: | No | 30 | 2 or more | Minor Approach 4: | Westbound E Center St |

| | | Major | Major | Total | Warra | nt Met | Minor | Minor | Largest | Warra | nt Met | Met San | ne Hours | Combi | nation | MWS | 6A (C) |
|--------------------|-------------|-----------------|--------------|--------|-------|--------|------------|------------|------------|---------|----------------|-------------|---------------|----------|----------|-----|--------|
| () | Hour | Approach 1 | Approach 3 | 1+3 | 600 | 900 | Approach 2 | Approach 4 | Minor App. | 200 | 100 | Condition A | Condition B | Α | В | 300 | 200 |
| 15 | 6 - 7 AM | 133 | 247 | 380 | | | 147 | 211 | 211 | Х | Х | | | | | Χ | Х |
| and | 7 - 8 AM | 290 | 520 | 810 | X | | 350 | 310 | 350 | X | Х | Х | | X | X | Х | Х |
| 1 B, % | 8 - 9 AM | 251 | 441 | 692 | X | | 272 | 200 | 272 | X | X | Х | | X | | X | Χ |
| | 9 - 10 AM | 222 | 373 | 595 | | | 266 | 166 | 266 | X | X | | | X | | X | Х |
| ₹ | 10 - 11 AM | 198 | 325 | 523 | | | 253 | 163 | 253 | X | Х | | | X | | Х | Х |
| | 11 - 12 AM | 237 | 337 | 574 | | | 204 | 204 | 204 | X | Х | | | X | | Х | Х |
| Warrants | 12 - 1 PM | 226 | 342 | 568 | | | 236 | 300 | 300 | X | X | | | X | | Х | Х |
| arı | 1 - 2 PM | 238 | 283 | 521 | | | 222 | 291 | 291 | X | X | | | X | | X | Х |
| | 2-3 PM | 287 | 367 | 654 | X | | 272 | 292 | 292 | X | X | Х | | X | | Х | Х |
| . <u>is</u> | 3 - 4 PM | 350 | 515 | 865 | X | | 460 | 311 | 460 | X | X | X | | X | X | X | X |
| Warrants Analysis: | 4 - 5 PM | 328 | 430 | 758 | X | | 465 | 325 | 465 | X | X | X | | X | X | X | X |
| na | 5-6 PM | 348 | 417 | 765 | X | | 416 | 258 | 416 | X | X | Х | | X | X | X | X |
| Α σ | 6 - 7 PM | 275 | 311 | 586 | | | 204 | 195 | 204 | X | X | | | X | | X | X |
| Ĕ | 7 - 8 PM | 190 | 229 | 419 | | | 132 | 87 | 132 | | X | | | | | X | X |
| ırs | 8 - 9 PM | 191 | 174 | 365 | | | 116 | 76 | 116 | | Х | | | | | X | |
| ⊗ | 9 - 10 PM | 125 | 123 | 248 | | | 88 | 56 | 88 | | | | | | | | |
| | 10 - 11 PM | 0 | 0 | 0 | | | 0 | 0 | 0 | | | 6 | 0 | 12 | 4 | | 4 |
| | | Warrant | and Descript | ion | | | Hours | Mot | Houre | Require | ad . | U | · | t/Not Me | | | 4 |
| | MWSA (C): | Multiway Stop | | | on C | | 1/2 | | Hours | 8 | , u | | Met - Multiwa | | | ns | |
| Warrant Summary | . , | Minimum Veh | | | 011 0 | | 6 | r | | 8 | | | | Not Met | фрисацо | 110 | |
| Warrant | | Interruption of | | | | | 0 | | | 8 | | | | Not Met | | | |
| L Aal | | Combination | | 101110 | | | 4 | | | 8 | | | | Not Met | | | |
| > \(\bar{s}\) | Warrant 2: | Four-Hour Ve | | е | | | 4 | | | 4 | | | Met - Wa | | atisfied | | |
| | Warrant 3B: | | | - | | | 1 | | | 1 | | | Met - War | | | | |



Forecasted Year 2040

11th Ave SE at E Center St Intersection Control Evaluation City of Rochester, Olmstead County



Number of Hours Satisfying Requirements:

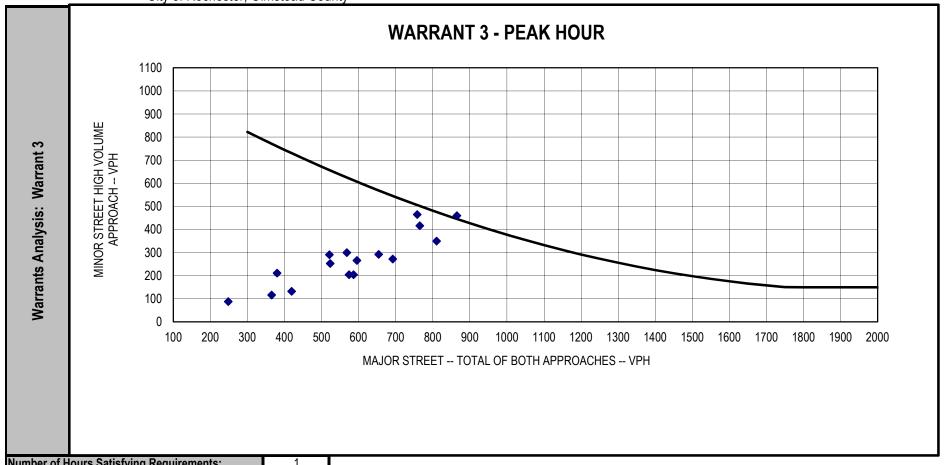
Notes:

1. 115 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACH WITH TWO OR MORE LANES AND 80 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.



Forecasted Year 2040

11th Ave SE at E Center St Intersection Control Evaluation City of Rochester, Olmstead County



Number of Hours Satisfying Requirements:

Notes:

1. 150 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACH WITH TWO OR MORE LANES AND 100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Signal Warrant Analysis - 80% Removal Criteria



80% Signal Removal Criteria

11th Ave SE at E Center St Intersection Control Evaluation City of Rochester, Olmstead County

| pr u | Location: City of Rochester, Olmste | ad County | Speed (mph) | Lanes | Approach | | | | |
|---------|-------------------------------------|-----------|-------------|-----------|-------------------|------------------------|--|--|--|
| 를 했다. | Date: 10/24/2018 | | 30 | 2 | Major Approach 1: | Northbound 11th Ave SE | | | |
| gra | Analysis Prepared By: Kevin Olm | | 30 | 2 | Major Approach 3: | Southbound 11th Ave SE | | | |
| 호호 | Population Less than 10,000: | No | 30 | 2 or more | Minor Approach 2: | Eastbound E Center St | | | |
| Ba | Seventy Percent Factor Used: | No | 30 | 2 or more | Minor Approach 4: | Westbound E Center St | | | |

| | | Major | Major | Total | Warra | nt Met | Minor | Minor | Largest | Warra | nt Met | Met San | ne Hours | Comb | ination | MWS | A (C) |
|--------------------|--|---------------|----------------|-----------|-------|--------|------------|------------|------------|---------|---------|-------------|---------------|-----------|-------------|-----|-------|
| () | Hour | Approach 1 | Approach 3 | 1+3 | 480 | 720 | Approach 2 | Approach 4 | Minor App. | 160 | 80 | Condition A | Condition B | Α | В | 300 | 200 |
| 10 | 6 - 7 AM | 123 | 195 | 318 | | | 91 | 184 | 184 | Χ | Х | | | | | Х | Х |
| and | 7 - 8 AM | 268 | 410 | 678 | Χ | | 216 | 270 | 270 | Х | Х | Х | | Х | Х | X | Х |
| 1B a | 8 - 9 AM | 232 | 348 | 580 | Χ | | 168 | 174 | 174 | Х | Х | Х | | Х | Х | X | Х |
| Ź | 9 - 10 AM | 205 | 294 | 499 | Χ | | 164 | 145 | 164 | Х | Х | Х | | Х | | X | Х |
| 4 | 10 - 11 AM | 183 | 256 | 439 | | | 156 | 142 | 156 | | Х | | | Х | | X | Х |
| ţs | 11 - 12 AM | 219 | 266 | 485 | X | | 126 | 178 | 178 | Х | Х | Х | | Х | | X | Х |
| Warrants | 12 - 1 PM | 205 | 303 | 508 | X | | 151 | 237 | 237 | Х | Х | Х | | Х | | X | Х |
| arı, | 1 - 2 PM | 216 | 251 | 467 | | | 142 | 230 | 230 | Х | Х | | | Х | | X | Х |
| | 2 - 3 PM | 260 | 325 | 585 | Χ | | 174 | 231 | 231 | Х | Х | Х | | Х | Х | X | Х |
| . <u>::</u> | 3 - 4 PM | 317 | 456 | 773 | X | X | 294 | 246 | 294 | Х | Х | Х | Х | Х | Х | X | Х |
| Warrants Analysis: | 4 - 5 PM | 297 | 381 | 678 | X | | 297 | 257 | 297 | Х | Х | Х | | Х | Х | X | Х |
| na | 5-6 PM | 315 | 369 | 684 | Χ | | 266 | 204 | 266 | Х | Х | Х | | Х | Х | X | Х |
| ∀ | 6-7 PM | 249 | 275 | 524 | X | | 130 | 154 | 154 | | Х | | | Х | | X | Х |
| ij | 7 - 8 PM | 172 | 203 | 375 | | | 84 | 69 | 84 | | Х | | | | | X | |
| rra | 8-9 PM | 173 | 154 | 327 | | | 74 | 60 | 74 | | | | | | | X | |
| Na | 9 - 10 PM | 113 | 109 | 222 | | | 56 | 44 | 56 | | | | | | | | |
| | 10 - 11 PM | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | 9 | 1 | 12 | 6 | 1 | 3 |
| | | | and Descript | ion | | | Hours | Met | Hours | Require | d | | | t/Not M | | | |
| > | Warrant 1A: Minimum Vehicular Volume | | | | | 9 | | | 8 | | | Met - War | | Satisfied | | | |
| Warrant Summary | Warrant 1B: Interruption of Continuous Traffic | | | | 1 | | | 8 | | | | Not Met | | | | | |
| arr un | Warrant 1C: Combination of Warrants | | | 6 | | 8 | | Not Met | | | | | | | | | |
| l ≋ ing | Warrant 2: Four-Hour Vehicular Volume | | | | 1 | 4 | | | Not Met | | | | | | | | |
| | | Peak Hour | | | | | 0 1 | | | | Not Met | | | | | | |
| | MWSA (C): | Multiway Stop | Applications (| Condition | on C | | 13 | 3 | | 8 | | | Met - Multiwa | ay Stop | Application | ons | |

Detailed 2018 Operations Analysis

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All |
|--------------------|------|------|-----|-----|-----|
| Denied Delay (hr) | 0.0 | 0.1 | 0.0 | 0.1 | 0.2 |
| Denied Del/Veh (s) | 0.6 | 1.1 | 0.4 | 8.0 | 0.7 |
| Total Delay (hr) | 1.3 | 1.4 | 0.1 | 0.3 | 3.1 |
| Total Del/Veh (s) | 19.8 | 19.1 | 1.5 | 2.7 | 9.3 |

| Denied Delay (hr) | 0.2 | |
|--------------------|------|--|
| Denied Del/Veh (s) | 0.7 | |
| Total Delay (hr) | 3.6 | |
| Total Del/Veh (s) | 10.6 | |

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All |
|--------------------|------|------|-----|-----|------|
| Denied Delay (hr) | 0.1 | 0.1 | 0.0 | 0.1 | 0.3 |
| Denied Del/Veh (s) | 1.2 | 1.6 | 0.3 | 0.6 | 0.9 |
| Total Delay (hr) | 2.6 | 1.6 | 0.2 | 0.3 | 4.6 |
| Total Del/Veh (s) | 31.3 | 20.4 | 1.8 | 2.2 | 12.3 |

| Denied Delay (hr) | 0.3 | |
|--------------------|------|--|
| Denied Del/Veh (s) | 0.9 | |
| Total Delay (hr) | 5.1 | |
| Total Del/Veh (s) | 13.5 | |

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All |
|--------------------|------|-----|------|------|------|
| Denied Delay (hr) | 0.0 | 0.1 | 0.0 | 0.1 | 0.2 |
| Denied Del/Veh (s) | 0.6 | 1.1 | 0.4 | 8.0 | 0.7 |
| Total Delay (hr) | 0.7 | 0.7 | 0.9 | 2.1 | 4.3 |
| Total Del/Veh (s) | 10.6 | 9.7 | 11.8 | 16.7 | 12.9 |

| 0.2 | |
|------|-----|
| 0.7 | |
| 5.0 | |
| 15.0 | |
| | 5.0 |

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All | |
|--------------------|------|-----|------|------|------|--|
| Denied Delay (hr) | 0.1 | 0.1 | 0.0 | 0.1 | 0.3 | |
| Denied Del/Veh (s) | 1.2 | 1.6 | 0.4 | 0.7 | 0.9 | |
| Total Delay (hr) | 0.9 | 0.7 | 1.5 | 2.9 | 5.9 | |
| Total Del/Veh (s) | 10.3 | 9.2 | 16.1 | 22.6 | 15.6 | |

| Denied Delay (hr) | 0.3 | |
|--------------------|------|--|
| Denied Del/Veh (s) | 0.9 | |
| Total Delay (hr) | 6.7 | |
| Total Del/Veh (s) | 17.6 | |

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All | |
|--------------------|------|-----|-----|-----|-----|--|
| Denied Delay (hr) | 0.0 | 0.0 | 0.1 | 0.2 | 0.3 | |
| Denied Del/Veh (s) | 0.5 | 0.4 | 0.9 | 1.6 | 1.0 | |
| Total Delay (hr) | 0.7 | 0.7 | 0.6 | 1.1 | 3.0 | |
| Total Del/Veh (s) | 10.4 | 9.4 | 7.5 | 8.7 | 8.9 | |

| Denied Delay (hr) | 0.3 |
|--------------------|------|
| Denied Del/Veh (s) | 1.0 |
| Total Delay (hr) | 3.5 |
| Total Del/Veh (s) | 10.5 |

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All | |
|--------------------|------|-----|-----|-----|-----|--|
| Denied Delay (hr) | 0.1 | 0.0 | 0.1 | 0.2 | 0.3 | |
| Denied Del/Veh (s) | 0.7 | 0.4 | 0.9 | 1.2 | 0.9 | |
| Total Delay (hr) | 0.9 | 0.7 | 8.0 | 1.1 | 3.6 | |
| Total Del/Veh (s) | 10.5 | 9.7 | 9.1 | 9.0 | 9.5 | |

| Denied Delay (hr) | 0.3 | |
|--------------------|------|--|
| Denied Del/Veh (s) | 0.9 | |
| Total Delay (hr) | 4.2 | |
| Total Del/Veh (s) | 11.1 | |

F.27.b

| | | | | HCS | 7 Ro | und | abo | uts R | lepo | rt | | | | | | | Ľ |
|--|----------------------|-----------|--------|----------|-------|------|---------------------------------|------------|-------|------|-----|--------|------------|---------|---------|--------|--------|
| General Information | | | | | | | Site | Info | mati | on | _ | | | | | | |
| Analyst | Kevin | Olm | | | | | Inte | ersection | | | | 11th A | ve at E Ce | enter S | nter St | | |
| Agency or Co. | SRF C | Consultin | g | | | | E/W | √ Street N | lame | | | E Cent | er Street | t | | | |
| Date Performed | 10/16 | 5/2018 | | | | | N/S Street Name 11th Avenue SE | | | | | | | | | | |
| Analysis Year | 2018 | | | | | | Analysis Time Period (hrs) 0.25 | | | | | | | | | | |
| Time Analyzed | AM | | | | | | Peak Hour Factor 0.88 | | | | | | | | | | |
| Project Description | ICE R | eport | | | | | Juri | sdiction | | | | | | | | | |
| Volume Adjustments | s and | Site C | harac | teristic | :s | | | | | | | | | | | | |
| Approach | | E | B | | | ٧ | VB | | | | NI | В | | | | SB | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | | Т | R | U | L | Т | R |
| Number of Lanes (N) | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | C | | 1 | 0 | 0 | 0 | 1 | 0 |
| Lane Assignment | | | Lī | ΓR | | | | LTR | | | | LTI | R | | | | LTR |
| Volume (V), veh/h | 0 | 16 | 189 | 19 | 0 | 10 | 190 | 57 | 0 | 4 | 9 | 208 | 9 | 0 | 145 | 247 | 45 |
| Percent Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | | 2 | 2 | 2 | 2 | 2 | 2 |
| Flow Rate (VPCE), pc/h | 0 | 19 | 219 | 22 | 0 | 12 | 220 | 66 | 0 | 5 | 7 | 241 | 10 | 0 | 168 | 286 | 52 |
| Right-Turn Bypass | | None | | | | | one | | | | No | ne | | | 1 | Vone | |
| Conflicting Lanes | | | 1 | | | | 1 | | | | 1 | | | | | 1 | |
| Pedestrians Crossing, p/h | ians Crossing, p/h 0 | | | | | | 0 | | | | 0 | | | | | 0 | |
| Critical and Follow-U | Јр Не | adway | / Adju | stmen | t | | | | | | | | | | | | |
| Approach | | | | EB | | Т | | WB | | Т | | NB | | Т | | SB | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | Bypas | s Le | ft | Right | Bypas | s L | Left | Right | Bypass |
| Critical Headway (s) | | | | 4.9763 | | | \neg | 4.9763 | | | | 4.9763 | | Т | | 4.9763 | |
| Follow-Up Headway (s) | | | | 2.6087 | | | | 2.6087 | | | | 2.6087 | | Т | | 2.6087 | |
| Flow Computations, | Capa | city ar | nd v/c | Ratio | 5 | | | | | | | | | | | | |
| Approach | | | | EB | | | | WB | | | | NB | | Т | | SB | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | Bypas | s Le | ft | Right | Bypas | s L | Left | Right | Bypass |
| Entry Flow (v _e), pc/h | | | | 260 | | | | 298 | | | | 308 | | Т | | 506 | |
| Entry Volume veh/h | | | | 255 | | | | 292 | | | | 302 | | Т | | 496 | |
| Circulating Flow (v _c), pc/h | | | | 466 | | | | 317 | | | | 406 | | | | 289 | |
| Exiting Flow (vex), pc/h | | | | 397 | | | | 329 | | | | 326 | | | | 320 | |
| Capacity (c _{pce}), pc/h | | | | 858 | | | | 999 | | | | 912 | | | | 1028 | |
| Capacity (c), veh/h | | | | 841 | | | | 979 | | | | 894 | | | | 1008 | |
| v/c Ratio (x) | | | | 0.30 | | | | 0.30 | | | | 0.34 | | | | 0.49 | |
| Delay and Level of S | ervice | • | | | | | | | | | | | | | | | |
| Approach | | | | EB | | | | WB | | | | NB | | Т | | SB | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | Bypas | s Le | ft | Right | Bypas | s L | Left | Right | Bypass |
| Lane Control Delay (d), s/veh | | | | 7.6 | | | | 6.7 | | | | 7.8 | | | | 9.4 | |
| Lane LOS | | | | А | | | | Α | | | | А | | | | Α | |
| 95% Queue, veh | 95% Queue, veh | | | 1.3 | | | | 1.3 | | | | 1.5 | | | | 2.8 | |
| Approach Delay, s/veh | | | 7.6 | | | | 6.7 | | | | 7.8 | | | | 9.4 | | |
| Approach LOS | | | | Α | | A | | | | | | Α | | | | Α | |
| Intersection Delay, s/veh LOS | | | | | | 8.1 | | | | | | | | Α | | | |

F.27.b

| | | | | HCS | 7 Ro | und | abo | uts R | lepo | rt | | | | | | ۳ | |
|--|-----------------------------|-----------|--------|----------|-------|------|---------------------------------|------------|--------|--------|------|------------|-------|---|---|--------|--|
| General Information | | | | | | | Site | Infor | mati | on | | | | | | | |
| Analyst | Kevin | Olm | | | | | Inte | rsection | | | 11th | Ave at E | Cente | er St | | | |
| Agency or Co. | SRF C | Consultin | g | | | | E/W | / Street N | lame | | E Ce | nter Stree | et | | | | |
| Date Performed | 10/16 | 5/2018 | | | | | N/S Street Name 11th Avenue SE | | | | | | SE | | | | |
| Analysis Year | 2018 | | | | | | Analysis Time Period (hrs) 0.25 | | | | | | | | | | |
| Time Analyzed | PM | | | | | | Peak Hour Factor 0.88 | | | | | | | | | | |
| Project Description | ICE R | eport | | | | | Juris | sdiction | | | | | | | | | |
| Volume Adjustments | s and | Site C | harac | teristic | cs | | | | | | | | | | | | |
| Approach | | E | EB | | | ٧ | VB | | Т | | NB | | | | SB | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | |
| Number of Lanes (N) | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | |
| Lane Assignment | | | Ľ | ΓR | | | | LTR | | | | .TR | | | | LTR | |
| Volume (V), veh/h | 0 | 44 | 173 | 91 | 0 | 11 | 159 | 96 | 0 | 51 | 261 | 6 | 0 | 101 | 1 301 | 39 | |
| Percent Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | |
| Flow Rate (VPCE), pc/h | 0 | 51 | 201 | 105 | 0 | 13 | 184 | 111 | 0 | 59 | 303 | 7 | 0 | 117 | 7 349 | 45 | |
| Right-Turn Bypass | None | | | | | No | one | | | | None | | | | None | | |
| Conflicting Lanes | | | 1 | | | | 1 | | | | 1 | | | | 1 | | |
| Pedestrians Crossing, p/h | Pedestrians Crossing, p/h 0 | | | | 0 | | | | | 0 | | | | 0 | | | |
| Critical and Follow-U | Јр Не | adway | , Adju | stmen | ıt | | | | | | | | | | | | |
| Approach | | | | EB | | Т | | WB | | \top | NE | | Т | | SB | | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | Bypass | Left | Rigl | nt Bypa | ass | Left | Right | Bypass | |
| Critical Headway (s) | | | | 4.9763 | | Т | \neg | 4.9763 | | | 4.97 | 53 | T | | 4.9763 | | |
| Follow-Up Headway (s) | | | | 2.6087 | | | | 2.6087 | | | 2.60 | 37 | | | 2.6087 | | |
| Flow Computations, | Capa | city ar | nd v/c | Ratio | s | | | | | | | | | | | | |
| Approach | | | | EB | | Т | | WB | | | NE | | Т | | SB | | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | Bypass | Left | Rigl | nt Bypa | ass | Left | Right | Bypass | |
| Entry Flow (v _e), pc/h | | | | 357 | | | | 308 | | | 369 |) | | | 511 | | |
| Entry Volume veh/h | | | | 350 | | | | 302 | | | 362 | ! | | | 501 | | |
| Circulating Flow (v _c), pc/h | | | | 479 | | | | 413 | | | 369 |) | | | SB L T 0 1 1 1 1 1 1 1 1 1 | | |
| Exiting Flow (vex), pc/h | | | | 325 | | | | 288 | | | 46! | ; | | L T R 0 1 0 101 301 399 2 2 2 117 349 459 117 588 Left Right Bypas 4.9763 4.9763 511 501 256 467 1063 1042 | | | |
| Capacity (c _{pce}), pc/h | | | | 847 | | | | 906 | | | 94 | , | | | 1063 | | |
| Capacity (c), veh/h | | | | 830 | | | | 888 | | | 929 | | | | 1042 | | |
| v/c Ratio (x) | | | | 0.42 | | | | 0.34 | | | 0.3 | 9 | | | 0.48 | | |
| Delay and Level of S | ervice | • | | | | | | | | | | | | | | | |
| Approach | | | | EB | | | | WB | | Т | NE | | П | | SB | | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | Bypass | Left | Rigl | nt Bypa | ass | Left | Right | Bypass | |
| Lane Control Delay (d), s/veh | | | | 9.6 | | | | 7.8 | | | 8.3 | | | | 9.0 | | |
| Lane LOS | | | | А | | | | Α | | | А | | | | А | | |
| 95% Queue, veh | | | | 2.1 | | | | 1.5 | | | 1.9 | | | | 2.7 | | |
| Approach Delay, s/veh | | | 9.6 | | | | 7.8 | | | 8.3 | | | | 9.0 | | | |
| Approach LOS | | | | Α | A | | | | | А | | | | Α | | | |
| Intersection Delay, s/veh LOS | | | | | | 8.7 | | | | | | | A | | | | |

Project: ICE Renort
Scheme: 11th Ave SE at E C
F.27.b

Rodel-Win1 - Full Geometry

Operational Data

Main Geometry (ft)

Approach and Entry Geometry

| | | - | | | | | | | | |
|-----|-------------------|------------------------------|--------------------------|-----------------|------------------------|---------------------|---------------------|-----------------------|----------------------|-----------------------|
| Leg | Leg Names | Approach Bearing (deg) | Grade Separation G | Half Width V | Approach Lanes n | Entry Width E | Entry Lanes n | Flare Length L' | Entry Radius R | Entry Angle Phi |
| 1 | NB 11th Ave SE | 0 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 2 | WB E Center St | 90 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 3 | SB 11th Ave SE | 180 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 4 | EB E Center St | 270 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed Diameter D | Circulating Width C | Circulating Lanes nc | Exit Width Ex | Exit Lanes nex | Exit Half Width Vx | Exit Half Width Lanes nvx |
|-----|-------------------|----------------------------|---------------------------|----------------------------|---------------------|----------------------|--------------------------|---------------------------------|
| 1 | NB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 2 | WB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 3 | SB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 4 | EB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |

Project: ICE Report
Scheme: 11th Ave SE at E Ce F.27.b

Rodel-Win1 - Full Geometry

Traffic Flow Data (veh/hr)

2020 AM Peak Peak Hour Flows

| | | | | Turning Flows | F | Flow Modifiers | | | |
|-----|-------------------|--------|--------|---------------|--------|----------------|-------------|----------------|---------------------|
| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks % | Flow Factor | Peak Hour Factor |
| 1 | NB 11th Ave SE | 0 | 49 | 208 | 9 | 0 | 2.0 | 1.00 | 0.880 |
| 2 | WB E Center St | 0 | 10 | 190 | 57 | 0 | 2.0 | 1.00 | 0.880 |
| 3 | SB 11th Ave SE | 0 | 145 | 247 | 45 | 0 | 2.0 | 1.00 | 0.880 |
| 4 | EB E Center St | 0 | 16 | 189 | 19 | 0 | 2.0 | 1.00 | 0.880 |

Project: ICE Renort
Scheme: 11th Ave SE at E C
F.27.b

Rodel-Win1 - Full Geometry

Operational Results

2020 AM Peak - 60 minutes

Delays, Queues and Level of Service

| Leg Leg Names | Bypass | Average Delay (sec) | | | 95% Qu | eue (veh) | Level of Service | | | |
|---------------|----------------|---------------------|-------|--------|--------|-----------|------------------|-------|--------|-----|
| Leg | Leg Names | Туре | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | NB 11th Ave SE | None | 6.22 | | 6.22 | 1.51 | | Α | | Α |
| 2 | WB E Center St | None | 5.75 | | 5.75 | 1.33 | | Α | | Α |
| 3 | SB 11th Ave SE | None | 7.93 | | 7.93 | 3.30 | | Α | | Α |
| 4 | EB E Center St | None | 6.04 | | 6.04 | 1.23 | | Α | | Α |

Project: ICE Report
Scheme: 11th Ave SE at E C
F.27.b

Rodel-Win1 - Full Geometry

Operational Data

Main Geometry (ft)

Approach and Entry Geometry

| | | - | | | | | | | | |
|-----|-------------------|------------------------------|--------------------------|-----------------|------------------------|---------------------|---------------------|-----------------------|----------------------|-----------------------|
| Leg | Leg Names | Approach Bearing (deg) | Grade Separation G | Half Width V | Approach Lanes n | Entry Width E | Entry Lanes n | Flare Length L' | Entry Radius R | Entry Angle Phi |
| 1 | NB 11th Ave SE | 0 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 2 | WB E Center St | 90 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 3 | SB 11th Ave SE | 180 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 4 | EB E Center St | 270 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed Diameter D | Circulating Width C | Circulating Lanes nc | Exit Width Ex | Exit Lanes nex | Exit Half Width Vx | Exit Half Width Lanes nvx |
|-----|-------------------|----------------------------|---------------------------|----------------------------|---------------------|----------------------|--------------------------|---------------------------------|
| 1 | NB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 2 | WB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 3 | SB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 4 | EB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |

Project: ICE Report
Scheme: 11th Ave SE at E Ce F.27.b

Rodel-Win1 - Full Geometry

Traffic Flow Data (veh/hr)

2020 PM Peak Peak Hour Flows

| | | Turning | | Turning Flows | 3 | | Flow Modifiers | | | |
|-----|-------------------|---------|--------|---------------|--------|--------|----------------|----------------|---------------------|--|
| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks % | Flow Factor | Peak Hour Factor | |
| 1 | NB 11th Ave SE | 0 | 51 | 261 | 6 | 0 | 2.0 | 1.00 | 0.880 | |
| 2 | WB E Center St | 0 | 11 | 159 | 96 | 0 | 2.0 | 1.00 | 0.880 | |
| 3 | SB 11th Ave SE | 0 | 101 | 301 | 39 | 0 | 2.0 | 1.00 | 0.880 | |
| 4 | EB E Center St | 0 | 44 | 173 | 91 | 0 | 2.0 | 1.00 | 0.880 | |

Project: ICE Renort
Scheme: 11th Ave SE at E C. F.27.b

Rodel-Win1 - Full Geometry

Operational Results

2020 PM Peak - 60 minutes

Delays, Queues and Level of Service

| _ | | | | | | | | | | |
|-----|----------------|--------|-------|----------------|------|--------|-----------|-------|----------------|-----|
| Lon | Log Names | Bypass | Ave | erage Delay (s | sec) | 95% Qu | eue (veh) | L | evel of Servic | е |
| Leg | Leg Names | Туре | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | NB 11th Ave SE | None | 6.65 | | 6.65 | 1.95 | | Α | | Α |
| 2 | WB E Center St | None | 6.25 | | 6.25 | 1.52 | | Α | | Α |
| 3 | SB 11th Ave SE | None | 7.76 | | 7.76 | 3.24 | | Α | | Α |
| 4 | EB E Center St | None | 7.13 | | 7.13 | 2.07 | | Α | | Α |

Project: ICE Report
Scheme: 11th Ave SE at E Ce F.27.b

Rodel-Win1 - Full Geometry

Operational Data

Main Geometry (ft)

Approach and Entry Geometry

| | | - | | | | | | | | |
|-----|-------------------|------------------------------|--------------------------|-----------------|------------------------|---------------------|---------------------|-----------------------|----------------------|-----------------------|
| Leg | Leg Names | Approach Bearing (deg) | Grade Separation G | Half Width V | Approach Lanes n | Entry Width E | Entry Lanes n | Flare Length L' | Entry Radius R | Entry Angle Phi |
| 1 | NB 11th Ave SE | 0 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 2 | WB E Center St | 90 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 3 | SB 11th Ave SE | 180 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 4 | EB E Center St | 270 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed Diameter D | Circulating Width C | Circulating Lanes nc | Exit Width Ex | Exit Lanes nex | Exit Half Width Vx | Exit Half Width Lanes nvx |
|-----|-------------------|----------------------------|---------------------------|----------------------------|---------------------|----------------------|--------------------------|---------------------------------|
| 1 | NB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 2 | WB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 3 | SB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 4 | EB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |

Project: ICE Renort
Scheme: 11th Ave SE at E C
F.27.b

Rodel-Win1 - Full Geometry

Traffic Flow Data (veh/hr)

2020 AM Peak Peak Hour Flows

| | | | , | Turning Flows | 5 | | ı | Flow Modifie | rs |
|-----|-------------------|--------|--------|---------------|--------|--------|-------------|----------------|---------------------|
| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks % | Flow Factor | Peak Hour Factor |
| 1 | NB 11th Ave SE | 0 | 49 | 208 | 9 | 0 | 2.0 | 1.00 | 0.880 |
| 2 | WB E Center St | 0 | 10 | 190 | 57 | 0 | 2.0 | 1.00 | 0.880 |
| 3 | SB 11th Ave SE | 0 | 145 | 247 | 45 | 0 | 2.0 | 1.00 | 0.880 |
| 4 | EB E Center St | 0 | 16 | 189 | 19 | 0 | 2.0 | 1.00 | 0.880 |

Project: ICE Renort
Scheme: 11th Ave SE at E C
F.27.b

Rodel-Win1 - Full Geometry

Operational Results

2020 AM Peak - 60 minutes

Delays, Queues and Level of Service

| Log | Log Names | Bypass | | | | 95% Queue (veh) | | Level of Service | | |
|-----|----------------|--------|-------|--------|-------|-----------------|--------|------------------|--------|-----|
| Leg | Leg Names | Туре | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | NB 11th Ave SE | None | 9.64 | | 9.64 | 2.45 | | Α | | Α |
| 2 | WB E Center St | None | 8.55 | | 8.55 | 2.04 | | Α | | Α |
| 3 | SB 11th Ave SE | None | 14.52 | | 14.52 | 6.57 | | В | | В |
| 4 | EB E Center St | None | 9.22 | | 9.22 | 1.96 | | Α | | Α |

Project: ICE Report
Scheme: 11th Ave SE at E Ce F.27.b

Rodel-Win1 - Full Geometry

Operational Data

Main Geometry (ft)

Approach and Entry Geometry

| | | - | | | | | | | | |
|-----|-------------------|------------------------------|--------------------------|-----------------|------------------------|---------------------|---------------------|-----------------------|----------------------|-----------------------|
| Leg | Leg Names | Approach Bearing (deg) | Grade Separation G | Half Width V | Approach Lanes n | Entry Width E | Entry Lanes n | Flare Length L' | Entry Radius R | Entry Angle Phi |
| 1 | NB 11th Ave SE | 0 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 2 | WB E Center St | 90 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 3 | SB 11th Ave SE | 180 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 4 | EB E Center St | 270 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed Diameter D | Circulating Width C | Circulating Lanes nc | Exit Width Ex | Exit Lanes nex | Exit Half Width Vx | Exit Half Width Lanes nvx |
|-----|-------------------|----------------------------|---------------------------|----------------------------|---------------------|----------------------|--------------------------|---------------------------------|
| 1 | NB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 2 | WB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 3 | SB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 4 | EB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |

Project: ICE Report
Scheme: 11th Ave SE at E Ce F.27.b

Rodel-Win1 - Full Geometry

Traffic Flow Data (veh/hr)

2020 PM Peak Peak Hour Flows

| | | | | Turning Flows | 3 | | F | low Modifie | rs |
|-----|-------------------|--------|--------|---------------|--------|--------|-------------|----------------|---------------------|
| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks % | Flow Factor | Peak Hour Factor |
| 1 | NB 11th Ave SE | 0 | 51 | 261 | 6 | 0 | 2.0 | 1.00 | 0.880 |
| 2 | WB E Center St | 0 | 11 | 159 | 96 | 0 | 2.0 | 1.00 | 0.880 |
| 3 | SB 11th Ave SE | 0 | 101 | 301 | 39 | 0 | 2.0 | 1.00 | 0.880 |
| 4 | EB E Center St | 0 | 44 | 173 | 91 | 0 | 2.0 | 1.00 | 0.880 |

Project: ICE Renort
Scheme: 11th Ave SE at E C
F.27.b

Rodel-Win1 - Full Geometry

Operational Results

2020 PM Peak - 60 minutes

Delays, Queues and Level of Service

| Log | Log Names | Bypass | | | | 95% Queue (veh) | | Level of Service | | |
|-----|----------------|--------|-------|--------|-------|-----------------|--------|------------------|--------|-----|
| Leg | Leg Names | Туре | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | NB 11th Ave SE | None | 10.71 | | 10.71 | 3.31 | | В | | В |
| 2 | WB E Center St | None | 9.72 | | 9.72 | 2.47 | | Α | | Α |
| 3 | SB 11th Ave SE | None | 13.95 | | 13.95 | 6.29 | | В | | В |
| 4 | EB E Center St | None | 12.05 | | 12.05 | 3.72 | | В | | В |

Detailed 2040 Operations Analysis

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All |
|--------------------|------|------|-----|-----|------|
| Denied Delay (hr) | 0.0 | 0.1 | 0.0 | 0.1 | 0.3 |
| Denied Del/Veh (s) | 0.6 | 1.1 | 0.4 | 0.8 | 0.7 |
| Total Delay (hr) | 3.5 | 4.3 | 0.2 | 0.4 | 8.4 |
| Total Del/Veh (s) | 46.4 | 51.7 | 1.8 | 3.1 | 22.0 |

| 0.3 | |
|------|-----|
| 0.7 | |
| 9.0 | |
| 23.3 | |
| | 9.0 |

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All |
|--------------------|------|------|-----|-----|------|
| Denied Delay (hr) | 0.2 | 0.1 | 0.0 | 0.1 | 0.5 |
| Denied Del/Veh (s) | 2.0 | 1.5 | 0.4 | 0.8 | 1.1 |
| Total Delay (hr) | 10.0 | 3.8 | 0.2 | 0.4 | 14.4 |
| Total Del/Veh (s) | 98.8 | 45.9 | 2.1 | 2.8 | 33.8 |

| Denied Delay (hr) | 0.5 |
|--------------------|------|
| Denied Del/Veh (s) | 1.1 |
| Total Delay (hr) | 15.0 |
| Total Del/Veh (s) | 34.9 |

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All | |
|--------------------|------|------|------|------|------|--|
| Denied Delay (hr) | 0.0 | 0.1 | 0.0 | 0.1 | 0.3 | |
| Denied Del/Veh (s) | 0.6 | 1.1 | 0.4 | 0.8 | 8.0 | |
| Total Delay (hr) | 1.0 | 1.0 | 1.3 | 5.1 | 8.4 | |
| Total Del/Veh (s) | 13.1 | 11.6 | 15.8 | 36.6 | 22.0 | |

| Denied Delay (hr) | 0.3 | |
|--------------------|------|--|
| Denied Del/Veh (s) | 0.8 | |
| Total Delay (hr) | 9.2 | |
| Total Del/Veh (s) | 24.1 | |

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All |
|--------------------|------|------|------|------|------|
| Denied Delay (hr) | 0.1 | 0.1 | 0.0 | 0.4 | 0.7 |
| Denied Del/Veh (s) | 1.3 | 1.5 | 0.4 | 2.6 | 1.6 |
| Total Delay (hr) | 1.3 | 0.9 | 2.7 | 11.2 | 16.0 |
| Total Del/Veh (s) | 12.7 | 11.0 | 27.3 | 77.1 | 37.6 |

| Denied Delay (hr) | 0.7 |
|--------------------|------|
| Denied Del/Veh (s) | 1.6 |
| Total Delay (hr) | 17.0 |
| Total Del/Veh (s) | 39.5 |

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All | |
|--------------------|------|------|-----|------|------|--|
| Denied Delay (hr) | 0.0 | 0.0 | 0.1 | 0.2 | 0.4 | |
| Denied Del/Veh (s) | 0.5 | 0.4 | 1.0 | 1.7 | 1.0 | |
| Total Delay (hr) | 0.8 | 0.9 | 0.8 | 1.4 | 4.0 | |
| Total Del/Veh (s) | 11.0 | 11.0 | 9.2 | 10.3 | 10.3 | |

| Denied Delay (hr) | 0.4 |
|--------------------|------|
| Denied Del/Veh (s) | 1.0 |
| Total Delay (hr) | 4.6 |
| Total Del/Veh (s) | 12.1 |

3: 11th Ave SE & E Center St Performance by approach

| Approach | EB | WB | NB | SB | All |
|--------------------|------|-----|------|------|------|
| Denied Delay (hr) | 0.1 | 0.0 | 0.1 | 0.2 | 0.4 |
| Denied Del/Veh (s) | 0.8 | 0.4 | 0.9 | 1.3 | 0.9 |
| Total Delay (hr) | 1.1 | 8.0 | 1.0 | 1.6 | 4.5 |
| Total Del/Veh (s) | 11.1 | 9.8 | 10.0 | 11.3 | 10.7 |

| 0.4 | |
|------|------------|
| 0.9 | |
| 5.3 | |
| 12.3 | |
| | 0.9 5.3 |

F.27.b

| | | | | HCS | 7 Ro | und | abo | uts R | lepoi | t | | | | | | ۳ | | |
|--|----------------|---------|--------|-------------|-------|------|-------------------|-------------------------------|----------|-------|--------|-----------|-----|---------|--------|--------|--|--|
| General Information | | | | | | | | Site Information | | | | | | | | | | |
| Analyst | Kevin Olm | | | | | | | Intersection 11th Ave at E Ce | | | | | | nter St | | | | |
| Agency or Co. | SRF Consulting | | | | | | | E/W Street Name E Center S | | | | | | Street | | | | |
| Date Performed | 10/16 | 5/2018 | | | | | N/S Street Name 1 | | | | | Avenue SE | | | | | | |
| Analysis Year | 2040 | | | | | | Ana | alysis Tim | e Perioc | (hrs) | 0.25 | | | | | | | |
| Time Analyzed | AM | | | | | | Pea | k Hour F | actor | | 0.88 | | | | | | | |
| Project Description | ICE R | eport | | | | | Jurisdiction | | | | | | | | | | | |
| Volume Adjustments | s and | Site C | harac | teristic | :s | | | | | | | | | | | | | |
| Approach | | E | B | | | ٧ | VB | | T | N | IB | | | | SB | | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | | |
| Number of Lanes (N) | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | | |
| Lane Assignment | | | Lī | ΓR | | | | LTR | | | LT | R | | | | LTR | | |
| Volume (V), veh/h | 0 | 20 | 215 | 25 | 0 | 15 | 215 | 65 | 0 | 55 | 235 | 10 | 0 | 165 | 280 | 50 | | |
| Percent Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | | |
| Flow Rate (VPCE), pc/h | 0 | 23 | 249 | 29 | 0 | 17 | 249 | 75 | 0 | 64 | 272 | 12 | 0 | 191 | 325 | 58 | | |
| Right-Turn Bypass | | No | one | | | No | one | | | No | ne | | | Ν | lone | | | |
| Conflicting Lanes | | | 1 | | | | 1 | | | | 1 | | | | | | | |
| Pedestrians Crossing, p/h | 0 | | | | | 0 | | | | | 0 | | | | 0 | | | |
| Critical and Follow-U | Јр Не | adway | / Adju | stmen | t | | | | | | | | | | | | | |
| Approach | | | | EB | | Т | | WB | | | NB | | Т | | SB | | | |
| Lane | | | Left | Right Bypas | | s Le | eft | Right | Bypass | Left | Right | Bypas | s L | _eft | Right | Bypass | | |
| Critical Headway (s) | | | | 4.9763 | | | T | 4.9763 | | | 4.9763 | 3 | | | 4.9763 | | | |
| Follow-Up Headway (s) | | | | 2.6087 | | | | 2.6087 | | | 2.6087 | 7 | | | 2.6087 | | | |
| Flow Computations, | Capa | city ar | nd v/c | Ratio | s | | | | | | | | | | | | | |
| Approach | | | | EB | В | | | WB | | | NB | | Т | | SB | | | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | Bypass | Left | Right | Bypas | s L | _eft | Right | Bypass | | |
| Entry Flow (v _e), pc/h | | | | 301 | | | | 341 | | | 348 | | | | 574 | | | |
| Entry Volume veh/h | | | | 295 | | | | 334 | | | 341 | | | | 563 | | | |
| Circulating Flow (v _c), pc/h | | | | 533 | | | | 359 | | | | | 330 | | | | | |
| Exiting Flow (vex), pc/h | | | | 452 | | | | 371 | | | 370 | | | | 371 | | | |
| Capacity (c _{pce}), pc/h | | | | 801 | | | | 957 | | | 861 | | | | 986 | | | |
| Capacity (c), veh/h | | | | 786 | | | | 938 | | | 844 | | | | 966 | | | |
| v/c Ratio (x) | | | | 0.38 | | | | 0.36 | | | 0.40 | | | | 0.58 | | | |
| Delay and Level of S | ervice | • | | | | | | | | | | | | | | | | |
| Approach | | | | EB | | | | WB | | | NB | | Т | | SB | | | |
| Lane | | | Left | Right | Bypas | s Le | eft | Right | Bypass | Left | Right | Bypas | s L | _eft | Right | Bypass | | |
| Lane Control Delay (d), s/veh | | | | 9.2 | | | | 7.7 | | | 9.2 | | | | 11.7 | | | |
| Lane LOS | | | | А | | | | Α | | | А | | | | В | | | |
| 95% Queue, veh | | | | 1.8 | | | | 1.6 | | | 2.0 | | | | 3.9 | | | |
| Approach Delay, s/veh | | | | 9.2 | | | | 7.7 | | | 9.2 | | | 11.7 | | | | |
| Approach LOS | | | | Α | | | | Α | | | Α | | | | В | | | |
| Intersection Delay, s/veh LO | S | | | | | 9.8 | | | | | | | Α | | | | | |

F.27.b

| | | | | HCS | 7 Ro | und | abo | uts R | lepo | rt | | | | | | | | |
|--|-----------|-----------|--------|----------|-------------|------|---------------------------------|--------------------------------------|----------|---------|--------|-------|-----|------|--------|-------|--|--|
| General Information | | | | | | | Site Information | | | | | | | | | | | |
| Analyst | Kevin Olm | | | | | | | Intersection 11th Ave at E Center St | | | | | | St | | | | |
| Agency or Co. | SRF C | Consultin | g | | | | E/W Street Name E Center Street | | | | | | | | | | | |
| Date Performed | 10/16 | 5/2018 | | | | | N/S Street Name 11th Avenue SE | | | | | | | | | | | |
| Analysis Year | 2040 | | | | | | Ana | alysis Tim | e Period | l (hrs) | 0.25 | | | | | | | |
| Time Analyzed | PM | | | | | | Pea | k Hour F | actor | | 0.88 | | | | | | | |
| Project Description | ICE R | eport | | | | | Jurisdiction | | | | | | | | | | | |
| Volume Adjustments | s and | Site C | harac | teristic | :s | | | | | | | | | | | | | |
| Approach | | E | B | | | ٧ | VB | | Т | ı | NB | | | | SB | | | |
| Movement | U | L | Т | R | U | L | Т | R | U | L | Т | R | U | L | Т | R | | |
| Number of Lanes (N) | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | | |
| Lane Assignment | | | Ľ | ΓR | • | | | LTR | | • | נז | R | | | | LTR | | |
| Volume (V), veh/h | 0 | 50 | 195 | 105 | 0 | 15 | 180 | 110 | 0 | 60 | 295 | 10 | 0 | 115 | 340 | 45 | | |
| Percent Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | | |
| Flow Rate (VPCE), pc/h | 0 | 58 | 226 | 122 | 0 | 17 | 209 | 128 | 0 | 70 | 342 | 12 | 0 | 133 | 394 | 52 | | |
| Right-Turn Bypass | | No | one | | | N | one | | | N | one | | | | Vone | | | |
| Conflicting Lanes | | 1 1 | | | | | | | | | 1 | | | 1 | | | | |
| Pedestrians Crossing, p/h | | 0 | | | | | 0 | | | | 0 | | | | 0 | | | |
| Critical and Follow-U | Јр Не | adway | , Adju | stmen | t | | | | | | | | | | | | | |
| Approach | | | | EB | | Т | | WB | | Т | NB | | Т | | SB | | | |
| Lane | | | Left | Right | Right Bypas | | eft | Right | Bypass | Left | Right | Вурая | s l | Left | Right | Вурая | | |
| Critical Headway (s) | | | | 4.9763 | yr | | | 4.9763 | | | 4.9763 | 3 | Т | | 4.9763 | | | |
| Follow-Up Headway (s) | | | | 2.6087 | | | | 2.6087 | | | 2.608 | 7 | | | 2.6087 | | | |
| Flow Computations, | Capa | city ar | nd v/c | Ratio | 5 | | | | | | | _ | | | | | | |
| Approach | | | | EB | | Т | | WB | | T | NB | | Т | | SB | | | |
| Lane | | | Left | Right | Bypas | s L | eft | Right | Bypass | Left | Right | Вурая | s l | Left | Right | Вурая | | |
| Entry Flow (v _e), pc/h | | | | 406 | | | | 354 | | | 424 | | Т | | 579 | | | |
| Entry Volume veh/h | | | | 398 | | | | 347 | | | 416 | | 568 | | | | | |
| Circulating Flow (v _c), pc/h | | | | 544 | | | | 470 | | | 417 | | | | 296 | | | |
| Exiting Flow (vex), pc/h | | | | 371 | | | | 331 | | | 528 | | | | 533 | | | |
| Capacity (c _{pce}), pc/h | | | | 792 | | | | 854 | | | 902 | | | | 1020 | | | |
| Capacity (c), veh/h | | | | 777 | | | | 838 | | | 884 | | | | 1000 | | | |
| v/c Ratio (x) | | | | 0.51 | | | | 0.41 | | | 0.47 | | | | 0.57 | | | |
| Delay and Level of S | ervice | , | | | | | | | | | | | | | | | | |
| Approach | | | | EB | | Τ | | WB | | | NB | | Т | | SB | | | |
| Lane | | | Left | Right | Bypas | s L | eft | Right | Bypass | Left | Right | Bypas | s L | Left | Right | Вура | | |
| Lane Control Delay (d), s/veh | | | | 12.0 | | | | 9.4 | | | 10.0 | | | | 11.0 | | | |
| Lane LOS | | | | В | | | | Α | | | А | | | | В | | | |
| 95% Queue, veh | | | | 3.0 | | | | 2.1 | | | 2.6 | | | | 3.7 | | | |
| Approach Delay, s/veh | | | | 12.0 | - | | | 9.4 | | | 10.0 | | | 11.0 | | | | |
| Approach LOS | | | | В | | | | Α | | | А | | | | В | | | |
| Intersection Delay, s/veh LO | S | | | | | 10.7 | | | | | | | В | | | | | |

Project: ICE Renort
Scheme: 11th Ave SE at E C
F.27.b

Rodel-Win1 - Full Geometry

Operational Data

Main Geometry (ft)

Approach and Entry Geometry

| Leg | Leg Names | Approach Bearing (deg) | Grade Separation G | Half Width V | Approach Lanes n | Entry Width E | Entry Lanes n | Flare Length L' | Entry Radius R | Entry Angle Phi |
|-----|-------------------|------------------------------|--------------------------|-----------------|------------------------|---------------------|---------------------|-----------------------|----------------------|-----------------------|
| 1 | NB 11th Ave SE | 0 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 2 | WB E Center St | 90 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 3 | SB 11th Ave SE | 180 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 4 | EB E Center St | 270 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed Diameter D | Circulating Width C | Circulating Lanes nc | Exit Width Ex | Exit Lanes nex | Exit Half Width Vx | Exit Half Width Lanes nvx |
|-----|-------------------|----------------------------|---------------------------|----------------------------|---------------------|----------------------|--------------------------|---------------------------------|
| 1 | NB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 2 | WB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 3 | SB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 4 | EB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |

Rodel-Win1 - Full Geometry

Traffic Flow Data (veh/hr)

2040 AM Peak Peak Hour Flows

| | | | | Turning Flows | 3 | | Flow Modifiers | | | | |
|-----|-------------------|--------|--------|---------------|--------|--------|----------------|----------------|---------------------|--|--|
| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks % | Flow Factor | Peak Hour Factor | | |
| 1 | NB 11th Ave SE | 0 | 55 | 235 | 10 | 0 | 2.0 | 1.00 | 0.880 | | |
| 2 | WB E Center St | 0 | 15 | 215 | 65 | 0 | 2.0 | 1.00 | 0.880 | | |
| 3 | SB 11th Ave SE | 0 | 165 | 280 | 50 | 0 | 2.0 | 1.00 | 0.880 | | |
| 4 | EB E Center St | 0 | 20 | 215 | 25 | 0 | 2.0 | 1.00 | 0.880 | | |

Rodel-Win1 - Full Geometry

Operational Results

2040 AM Peak - 60 minutes

| Log | Log Namoo | Bypass | Ave | erage Delay (s | sec) | 95% Queue (veh) | | Level of Service | | |
|-----|----------------|--------|-------|----------------|------|-----------------|--------|------------------|--------|-----|
| Leg | Leg Names | Туре | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | NB 11th Ave SE | None | 6.93 | | 6.93 | 1.94 | | Α | | Α |
| 2 | WB E Center St | None | 6.33 | | 6.33 | 1.71 | | Α | | Α |
| 3 | SB 11th Ave SE | None | 9.57 | | 9.57 | 4.70 | | Α | | Α |
| 4 | EB E Center St | None | 6.79 | | 6.79 | 1.65 | | Α | | Α |

Rodel-Win1 - Full Geometry

Operational Data

Main Geometry (ft)

Approach and Entry Geometry

| | | - | | | | | | | | |
|-----|-------------------|------------------------------|--------------------------|-----------------|------------------------|---------------------|---------------------|-----------------------|----------------------|-----------------------|
| Leg | Leg Names | Approach Bearing (deg) | Grade Separation G | Half Width V | Approach Lanes n | Entry Width E | Entry Lanes n | Flare Length L' | Entry Radius R | Entry Angle Phi |
| 1 | NB 11th Ave SE | 0 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 2 | WB E Center St | 90 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 3 | SB 11th Ave SE | 180 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 4 | EB E Center St | 270 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed Diameter D | Circulating Width C | Circulating Lanes nc | Exit Width Ex | Exit Lanes nex | Exit Half Width Vx | Exit Half Width Lanes nvx |
|-----|-------------------|----------------------------|---------------------------|----------------------------|---------------------|----------------------|--------------------------|---------------------------------|
| 1 | NB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 2 | WB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 3 | SB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 4 | EB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |

Rodel-Win1 - Full Geometry

Traffic Flow Data (veh/hr)

2040 PM Peak Peak Hour Flows

| | I a a Nama a | | | Turning Flows | 5 | | Flow Modifiers | | | | |
|-----|-------------------|--------|--------|---------------|--------|--------|----------------|----------------|---------------------|--|--|
| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks % | Flow Factor | Peak Hour Factor | | |
| 1 | NB 11th Ave SE | 0 | 60 | 295 | 10 | 0 | 2.0 | 1.00 | 0.880 | | |
| 2 | WB E Center St | 0 | 15 | 180 | 110 | 0 | 2.0 | 1.00 | 0.880 | | |
| 3 | SB 11th Ave SE | 0 | 115 | 340 | 45 | 0 | 2.0 | 1.00 | 0.880 | | |
| 4 | EB E Center St | 0 | 50 | 195 | 105 | 0 | 2.0 | 1.00 | 0.880 | | |

Rodel-Win1 - Full Geometry

Operational Results

2040 PM Peak - 60 minutes

| Log | Log Namoo | Bypass | Average Delay (sec) | | | 95% Queue (veh) | | Level of Service | | |
|-----|----------------|--------|---------------------|--------|------|-----------------|--------|------------------|--------|-----|
| Leg | Leg Names | Туре | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | NB 11th Ave SE | None | 7.61 | | 7.61 | 2.64 | | Α | | Α |
| 2 | WB E Center St | None | 7.03 | | 7.03 | 2.01 | | Α | | Α |
| 3 | SB 11th Ave SE | None | 9.32 | | 9.32 | 4.59 | | Α | | Α |
| 4 | EB E Center St | None | 8.31 | | 8.31 | 2.83 | | Α | | Α |

Rodel-Win1 - Full Geometry

Operational Data

Main Geometry (ft)

Approach and Entry Geometry

| Leg | Leg Names | Approach Bearing (deg) | Grade Separation G | Half Width V | Approach Lanes n | Entry Width E | Entry Lanes n | Flare Length L' | Entry Radius R | Entry Angle Phi |
|-----|-------------------|------------------------------|--------------------------|-----------------|------------------------|---------------------|---------------------|-----------------------|----------------------|-----------------------|
| 1 | NB 11th Ave SE | 0 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 2 | WB E Center St | 90 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 3 | SB 11th Ave SE | 180 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 4 | EB E Center St | 270 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed Diameter D | Circulating Width C | Circulating Lanes nc | Exit Width Ex | Exit Lanes nex | Exit Half Width Vx | Exit Half Width Lanes nvx |
|-----|-------------------|----------------------------|---------------------------|----------------------------|---------------------|----------------------|--------------------------|---------------------------------|
| 1 | NB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 2 | WB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 3 | SB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 4 | EB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |

Rodel-Win1 - Full Geometry

Traffic Flow Data (veh/hr)

2040 AM Peak Peak Hour Flows

| | I N | | | Turning Flows | 3 | | Flow Modifiers | | | | |
|-----|-------------------|--------|--------|---------------|--------|--------|----------------|----------------|---------------------|--|--|
| Leg | Leg Names | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks % | Flow Factor | Peak Hour Factor | | |
| 1 | NB 11th Ave SE | 0 | 55 | 235 | 10 | 0 | 2.0 | 1.00 | 0.880 | | |
| 2 | WB E Center St | 0 | 15 | 215 | 65 | 0 | 2.0 | 1.00 | 0.880 | | |
| 3 | SB 11th Ave SE | 0 | 165 | 280 | 50 | 0 | 2.0 | 1.00 | 0.880 | | |
| 4 | EB E Center St | 0 | 20 | 215 | 25 | 0 | 2.0 | 1.00 | 0.880 | | |

Rodel-Win1 - Full Geometry

Operational Results

2040 AM Peak - 60 minutes

| Log | Log Namoo | Bypass | Ave | erage Delay (s | sec) | 95% Queue (veh) | | Level of Service | | |
|-----|----------------|--------|-------|----------------|-------|-----------------|--------|------------------|--------|-----|
| Leg | Leg Names | Туре | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | NB 11th Ave SE | None | 11.47 | | 11.47 | 3.41 | | В | | В |
| 2 | WB E Center St | None | 9.90 | | 9.90 | 2.79 | | Α | | Α |
| 3 | SB 11th Ave SE | None | 21.18 | | 21.18 | 11.98 | | С | | С |
| 4 | EB E Center St | None | 11.07 | | 11.07 | 2.83 | | В | | В |

Rodel-Win1 - Full Geometry

Operational Data

Main Geometry (ft)

Approach and Entry Geometry

| | | - | | | | | | | | |
|-----|-------------------|------------------------------|--------------------------|-----------------|------------------------|---------------------|---------------------|-----------------------|----------------------|-----------------------|
| Leg | Leg Names | Approach Bearing (deg) | Grade Separation G | Half Width V | Approach Lanes n | Entry Width E | Entry Lanes n | Flare Length L' | Entry Radius R | Entry Angle Phi |
| 1 | NB 11th Ave SE | 0 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 2 | WB E Center St | 90 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 3 | SB 11th Ave SE | 180 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |
| 4 | EB E Center St | 270 | 0 | 12.00 | 1 | 17.00 | 1 | 5.00 | 22.00 | 40.00 |

Circulating and Exit Geometry

| Leg | Leg Names | Inscribed Diameter | Circulating Width | Circulating Lanes | Exit Width | Exit Lanes | Exit Half Width | Exit Half Width Lanes |
|-----|-------------------|-----------------------|----------------------|----------------------|---------------|---------------|--------------------|--------------------------|
| | | D | С | nc | Ex | nex | Vx | nvx |
| 1 | NB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 2 | WB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 3 | SB 11th Ave SE | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |
| 4 | EB E Center St | 70.00 | 18.00 | 1 | 15.00 | 1 | 12.00 | 1 |

Rodel-Win1 - Full Geometry

Traffic Flow Data (veh/hr)

2040 PM Peak Peak Hour Flows

| Leg | Leg Names | | | Turning Flows | Flow Modifiers | | | | |
|-----|-------------------|--------|--------|---------------|----------------|--------|-------------|----------------|---------------------|
| | | U-Turn | Exit-3 | Exit-2 | Exit-1 | Bypass | Trucks % | Flow Factor | Peak Hour Factor |
| 1 | NB 11th Ave SE | 0 | 60 | 295 | 10 | 0 | 2.0 | 1.00 | 0.880 |
| 2 | WB E Center St | 0 | 15 | 180 | 110 | 0 | 2.0 | 1.00 | 0.880 |
| 3 | SB 11th Ave SE | 0 | 115 | 340 | 45 | 0 | 2.0 | 1.00 | 0.880 |
| 4 | EB E Center St | 0 | 50 | 195 | 105 | 0 | 2.0 | 1.00 | 0.880 |

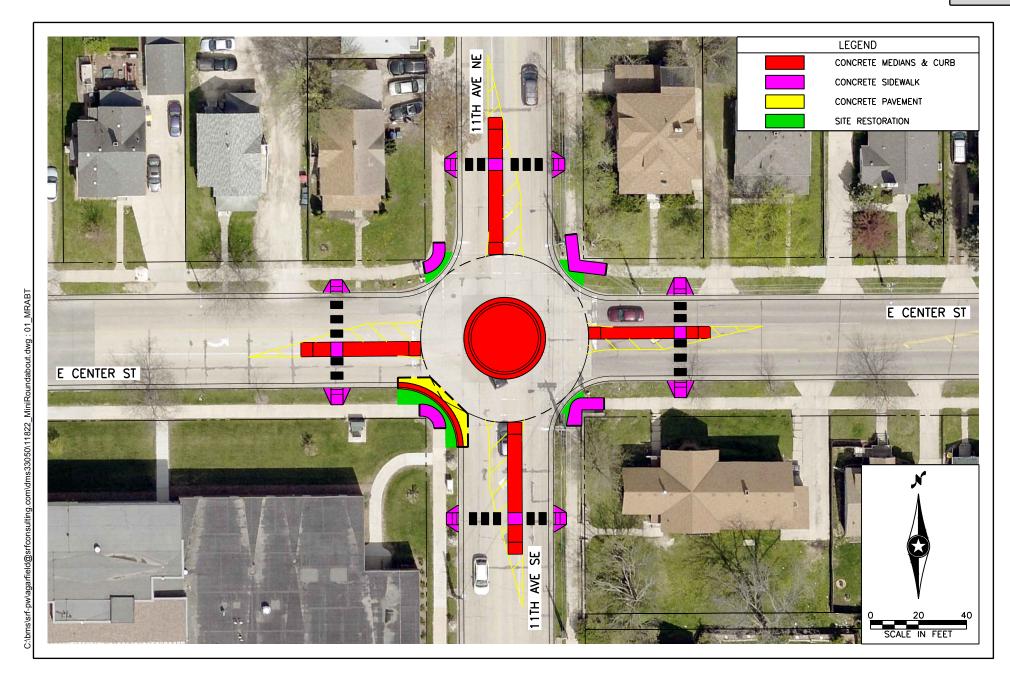
Rodel-Win1 - Full Geometry

Operational Results

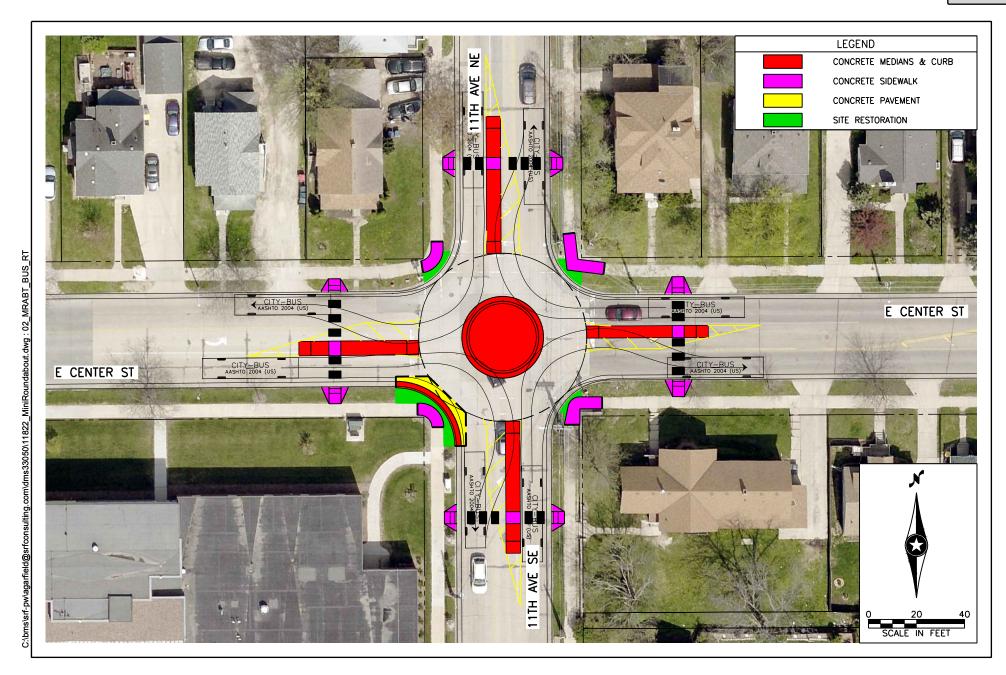
2040 PM Peak - 60 minutes

| Leg | Leg Names | Bypass Type | Average Delay (sec) | | | 95% Queue (veh) | | Level of Service | | |
|-----|----------------|----------------|---------------------|--------|-------|-----------------|--------|------------------|--------|-----|
| | | | Entry | Bypass | Leg | Entry | Bypass | Entry | Bypass | Leg |
| 1 | NB 11th Ave SE | None | 13.48 | | 13.48 | 5.04 | | В | | В |
| 2 | WB E Center St | None | 11.76 | | 11.76 | 3.58 | | В | | В |
| 3 | SB 11th Ave SE | None | 19.98 | | 19.98 | 11.20 | | С | | С |
| 4 | EB E Center St | None | 15.85 | | 15.85 | 5.95 | | С | | С |

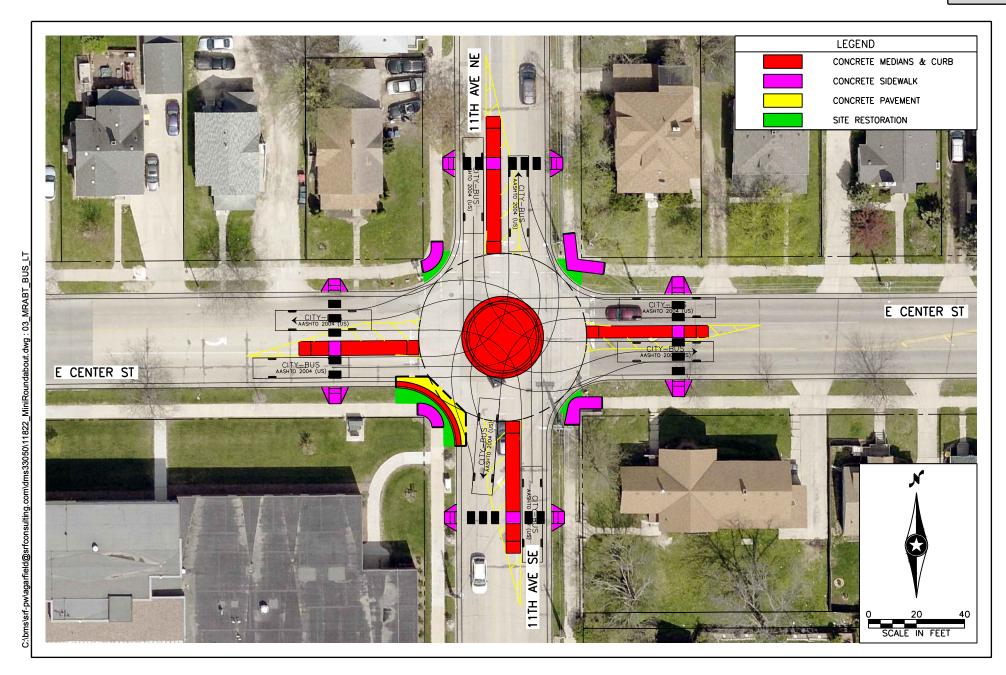
Mini-Roundabout Alternative Layout



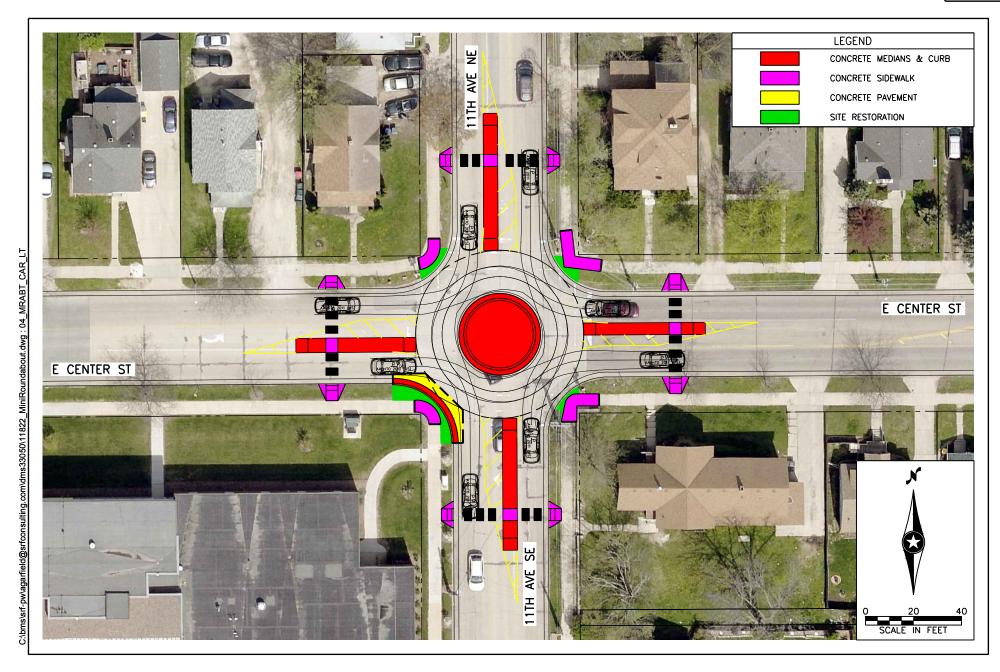














High-Level Cost Estimates

ALL-WAY STOP, TRAFFIC SIGNAL, AND MINI-ROUNDABOUT ROCHESTER, MN EAST CENTER STREET AND 11TH AVE SOUTHEAST SRF PROJECT NO. 11822 FEASIBILITY ESTIMATE

KAO 11/20/2018

| NOTES | ITEM NUMBER | | | ESTIMATED UNIT PRICE | SIDE-STREET/ALL-WAY STOP | | TRAFFIC SIGNAL | | MINI-ROUNDABOUT | |
|-------|-------------|---|----------|----------------------|--------------------------|-------------------|--------------------|-------------------|-----------------------|----------------|
| | | ITEM DESCRIPTION | UNIT | | ESTIMATED QUANTITY | ESTIMATED COST | ESTIMATED QUANTITY | ESTIMATED COST | ESTIMATED QUANTITY | ESTIMATED COST |
| | 2021.501 | MOBILIZATION | LUMP SUM | \$5,000.00 | 1 | \$5,000.00 | 1 | \$5,000.00 | 1 | \$5,000.00 |
| | 2102.518 | PAVEMENT MARKING REMOVAL | SQ FT | \$2.00 | 200 | \$400.00 | 0 | \$0.00 | 800 | \$1,600.00 |
| | | SAWING CONCRETE PAVEMENT (FULL DEPTH) | LIN FT | \$5.00 | 0 | \$0.00 | 0 | \$0.00 | 700 | \$3,500.00 |
| | | SAWING BITUMINOUS PAVEMENT (FULL DEPTH) | LIN FT | \$5.00 | 0 | \$0.00 | 0 | \$0.00 | 50 | \$250.00 |
| | 2104.503 | REMOVE CURB & GUTTER | LIN FT | \$5.00 | 0 | \$0.00 | 0 | \$0.00 | 150 | \$750.00 |
| | 2104.509 | REMOVE SIGNAL SYSTEM | EACH | \$10,000.00 | 1 | \$10,000.00 | 1 | \$10,000.00 | 1 | \$10,000.0 |
| | 2104.518 | REMOVE CONCRETE WALK | SQ FT | \$1.50 | 0 | \$0.00 | 0 | \$0.00 | 1300 | \$1,950.00 |
| | 2104.518 | REMOVE CONCRETE PAVEMENT | SQ FT | \$2.50 | 0 | \$0.00 | 0 | \$0.00 | 3150 | \$7,875.00 |
| | 2105.601 | MISCELLANEOUS TEMPORARY GRADING | LUMP SUM | \$5000.00 | 1 | \$5000.00 | 1 | \$5000.00 | 1 | \$5,000.00 |
| | 2106.507 | EXCAVATION - COMMON | CU YD | \$200.00 | 0 | \$0.00 | 0 | \$0.00 | 5 | \$1,000.00 |
| | 2106.507 | COMMON EMBANKMENT (CV) | CU YD | \$150.00 | 0 | \$0.00 | 0 | \$0.00 | 5 | \$750.00 |
| | 2123.610 | STREET SWEEPER (WITH PICKUP BROOM) | HOUR | \$150.00 | 0 | \$0.00 | 0 | \$0.00 | 5 | \$750.00 |
| | | AGGREGATE BASE (CV) CLASS 5 | CU YD | \$40.00 | 0 | \$0.00 | 0 | \$0.00 | 60 | \$2,400.0 |
| | 2301.504 | CONCRETE PAVEMENT 8.0" | SQ YD | \$60.00 | 0 | \$0.00 | 0 | \$0.00 | 70 | \$4,200.0 |
| | 2521.518 | 4" CONCRETE WALK | SQ FT | \$10.00 | 0 | \$0.00 | 0 | \$0.00 | 1800 | \$18,000.0 |
| | 2521.518 | 6" CONCRETE WALK | SQ FT | \$15.00 | 0 | \$0.00 | 0 | \$0.00 | 1350 | \$20,250.0 |
| | 2531.503 | CONCRETE CURB & GUTTER DESIGN D412 | LIN FT | \$30.00 | 0 | \$0.00 | 0 | \$0.00 | 360 | \$10.800.0 |
| | 2531.503 | CONCRETE CURB & GUTTER DESIGN B624 | LIN FT | \$40.00 | 0 | \$0.00 | 0 | \$0.00 | 130 | \$5,200.0 |
| | 2531.503 | CONCRETE CURB & GUTTER DESIGN D424 | LIN FT | \$40.00 | 0 | \$0.00 | 0 | \$0.00 | 100 | \$4,000.0 |
| | 2531.618 | TRUNCATED DOMES | SQ FT | \$50.00 | 0 | \$0.00 | 0 | \$0.00 | 40 | \$2,000.0 |
| | 2563.601 | TRAFFIC CONTROL (ALL-WAY STOP) | LUMP SUM | \$1,000.00 | 1 | \$1,000.00 | 0 | \$0.00 | 0 | \$0.00 |
| | 2563.601 | TRAFFIC CONTROL (TRAFFIC SIGNAL AND ROUNDABOUT) | LUMP SUM | \$2,500.00 | 0 | \$0.00 | 1 | \$2,500.00 | 1 | \$2,500.0 |
| | 2563.601 | DETOUR SIGNING | LUMP SUM | \$2,500.00 | 0 | \$0.00 | 0 | \$0.00 | 1 | \$2,500.0 |
| | | SIGN PANELS TYPE C | SQ FT | \$75.00 | 50 | \$3,750.00 | 0 | \$0.00 | 40 | \$3,000.0 |
| | 2565.516 | TRAFFIC CONTROL SIGNAL SYSTEM | SYS | \$200,000.00 | 0 | \$0.00 | 1 | \$200,000.00 | 0 | \$0.00 |
| | 2573.503 | SILT FENCE, TYPE MS | LIN FT | \$3.00 | 0 | \$0.00 | 0 | \$0.00 | 100 | \$300.00 |
| | 2575.602 | SITE RESTORATION | EACH | \$250.00 | 0 | \$0.00 | 0 | \$0.00 | 4 | \$1,000.0 |
| | 2582.503 | 4" BROKEN LINE MULTI COMP | LIN FT | \$6.00 | 0 | \$0.00 | 0 | \$0.00 | 80 | \$480.00 |
| | 2582.503 | 4" SOLID LINE MULTI COMP | LIN FT | \$6.00 | 0 | \$0.00 | 0 | \$0.00 | 800 | \$4,800.0 |
| | 2582.503 | 24" SOLID LINE MULTI COMP | LIN FT | \$12.00 | 50 | \$600.00 | 0 | \$0.00 | 0 | \$0.00 |
| | | CROSSWALK PAINT GR IN | SQ FT | \$15.00 | 300 | \$4,500.00 | 300 | \$4,500.00 | 300 | \$4,500.0 |
| | 2582.618 | PAVEMENT MARKING SPECIAL | SQ FT | \$0.30 | 70 | \$21.00 | 0 | \$0.00 | 0 | \$0.00 |
| | | +15% CONTINGENCY | | + + | | \$5,000.00 | | \$34,000.00 | | \$19,000.0 |
| | | +10% DESIGN | | | | \$3,000.00 | | \$23,000.00 | | \$12,000.0 |
| | | | | ROJECT TOTAL | £20.1 | 71.00 | 6204 | .000.00 | 6455 | 355.00 |

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